ECE 344
Microwave Fundamentals

Lecture 07:
Microwave Network Analysis
Multiport Networks

Prepared By

Dr. Sherif Hekal

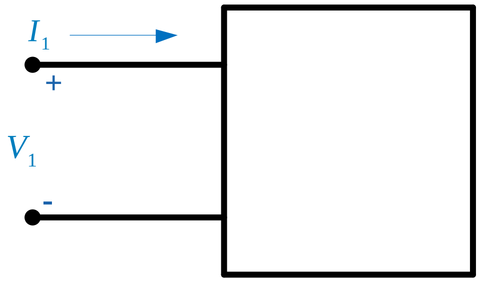
Multiport Networks

A general circuit can be represented by a multi-port network, where the "ports" are defined as access terminals at which we can define voltages and currents.

Examples:

Note: Equal and opposite currents are assumed on the two wires of a port.

1) One-port network



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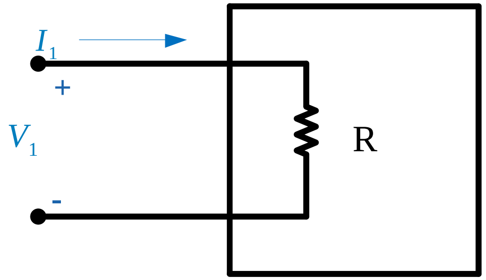
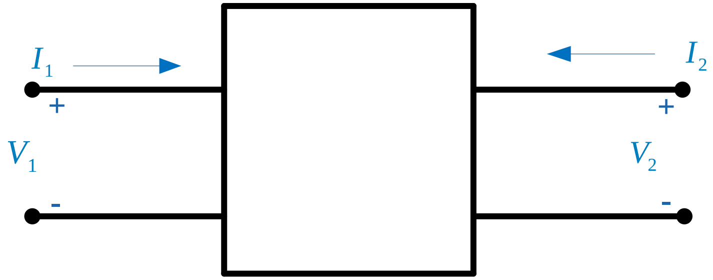


2) Two-port network



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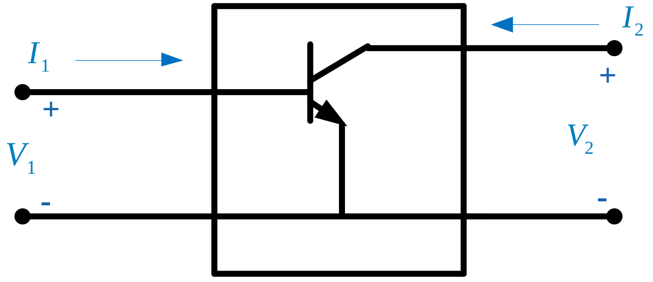


Multiport Networks (cont.)

3) N-port network

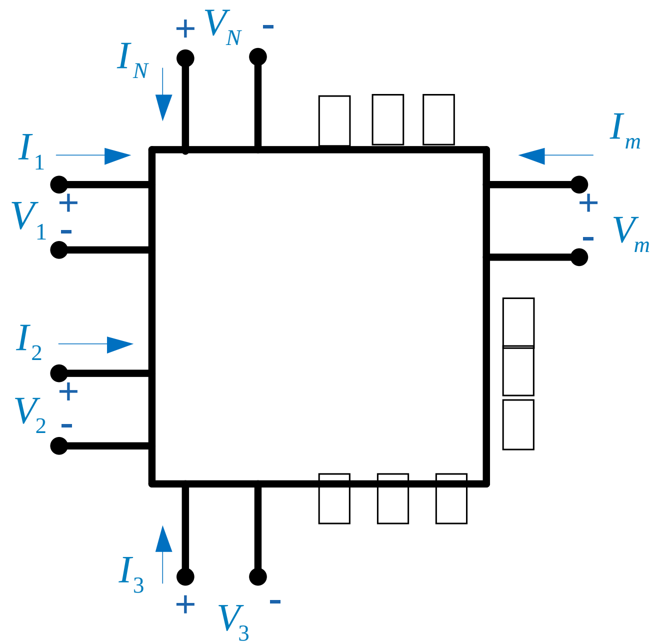
To represent multi-port networks we use:

- Z (impedance) parameters
- Y (admittance) parameters
- $ABCD$ parameters

Not easily measurable at high frequency

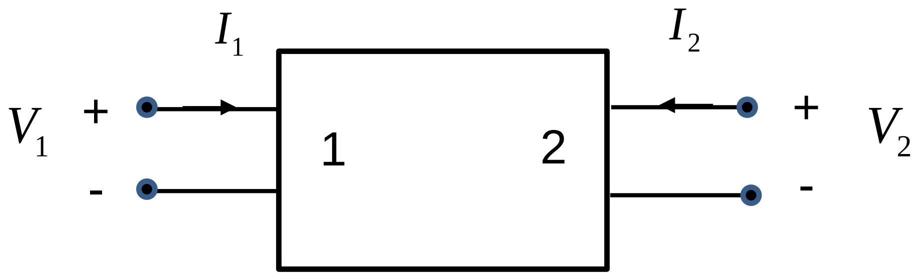
- S (scattering) parameters

Measurable at high frequency



Two-Port Networks

Consider a general 2-port linear network:



In terms of Z-parameters, we have (from superposition):

$$V_1 = Z_{11} I_1 + Z_{12} I_2$$
$$V_2 = Z_{21} I_1 + Z_{22} I_2$$

Impedance (Z) matrix

Therefore

$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} \Rightarrow [V] = [Z][I]$$

Elements of *Z*-Matrix: *Z*-Parameters

(open-circuit parameters)

$$V_1 = Z_{11} I_1 + Z_{12} I_2$$
$$V_2 = Z_{21} I_1 + Z_{22} I_2$$

Port 2 open circuited

$$Z_{11} = \left.\frac{V_1}{I_1}\right|_{I_2=0}$$

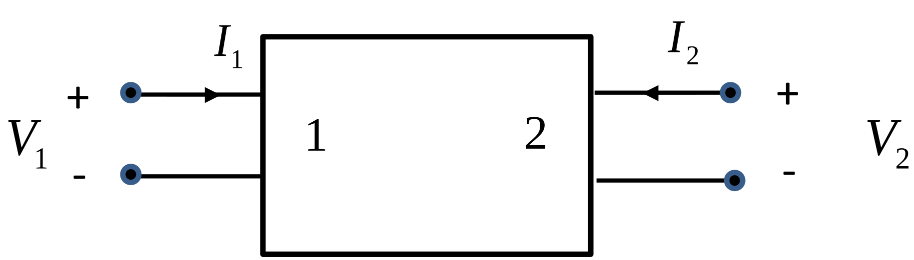
$$Z_{21} = \left.\frac{V_2}{I_1}\right|_{I_2=0}$$

$$\boxed{Z_{ij} = \left.\frac{V_i}{I_j}\right|_{I_k=0 \quad k \neq j}}$$

Port 1 open circuited

$$Z_{12} = \left.\frac{V_1}{I_2}\right|_{I_1=0}$$

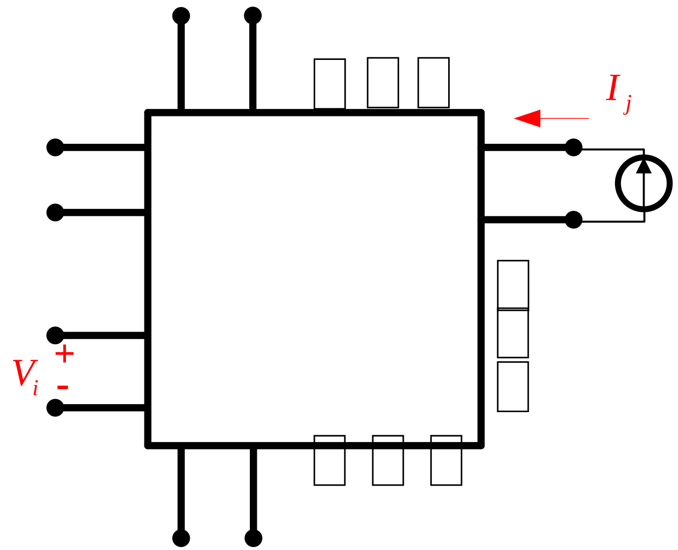
$$Z_{22} = \left.\frac{V_2}{I_2}\right|_{I_1=0}$$



Z-Parameters (cont.)

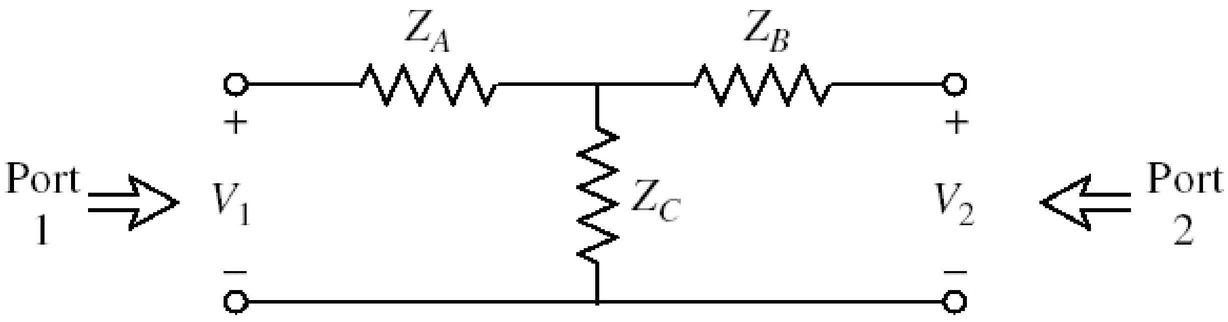
N-port network

$$Z_{ij} = \left. \frac{V_i}{I_j} \right|_{I_k = 0 \quad k \neq j}$$



We inject a current into port j and measure the voltage (with an ideal voltmeter) at port i. All ports are open-circuited except j.

Z-Parameters (cont.)



$$Z_{11} = \left.\frac{V_1}{I_1}\right|_{I_2=0} = ? \qquad Z_A + Z_C$$

$$Z_{22} = \left.\frac{V_2}{I_2}\right|_{I_1=0} = ? \qquad Z_B + Z_C$$

$$Z_{12} = \left.\frac{V_1}{I_2}\right|_{I_1=0} = ? \qquad Z_C$$

$$Z_{21} = \left.\frac{V_2}{I_1}\right|_{I_2=0} \overset{?}{=} Z_{12}$$

Z-Parameters (cont.)

Z-parameters are convenient for <u>series</u> connected networks.

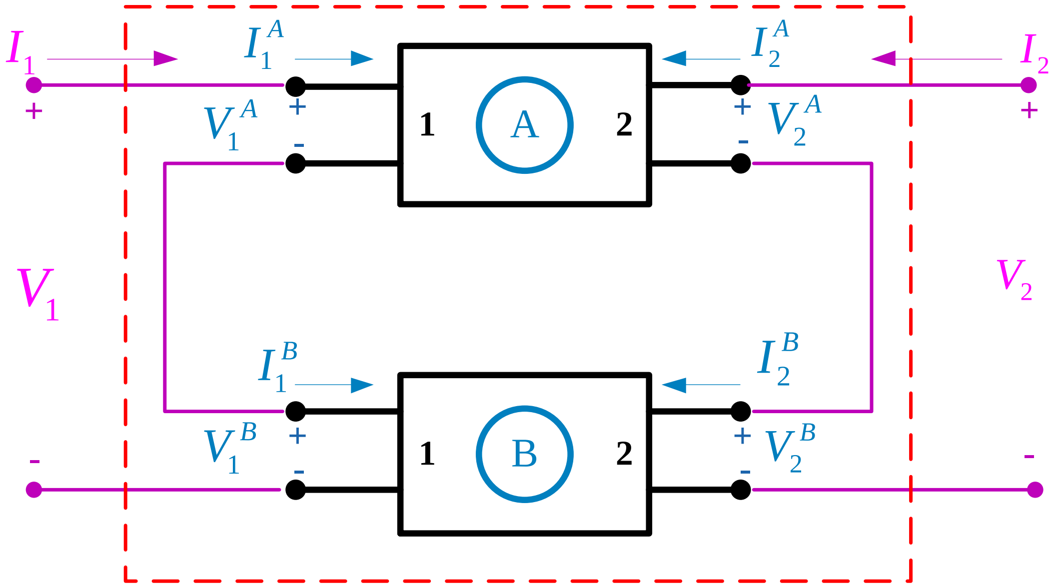
$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} V_1^A \\ V_2^A \end{bmatrix} + \begin{bmatrix} V_1^B \\ V_2^B \end{bmatrix}$$

$$= \left[Z^A\right]\left[I^A\right] + \left[Z^B\right]\left[I^B\right]$$

$$= \left(\left[Z^A\right] + \left[Z^B\right]\right)[I]$$

$$= \left(\left[Z^A\right] + \left[Z^B\right]\right)\begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$= \left[Z^A + Z^B\right]\begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$



$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} Z_{11}^A + Z_{11}^B & Z_{12}^A + Z_{12}^B \\ Z_{21}^A + Z_{21}^B & Z_{22}^A + Z_{22}^B \end{bmatrix}\begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

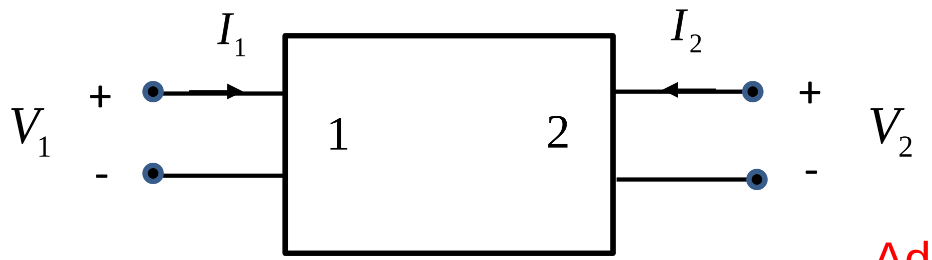
Series:

$$I_1 = I_1^A = I_1^B$$

$$I_2 = I_2^A = I_2^B$$

Admittance (Y) Parameters

Consider a linear 2-port network:



$$I_1 = Y_{11}V_1 + Y_{12}V_2$$
$$I_2 = Y_{21}V_1 + Y_{22}V_2$$

Admittance matrix

or

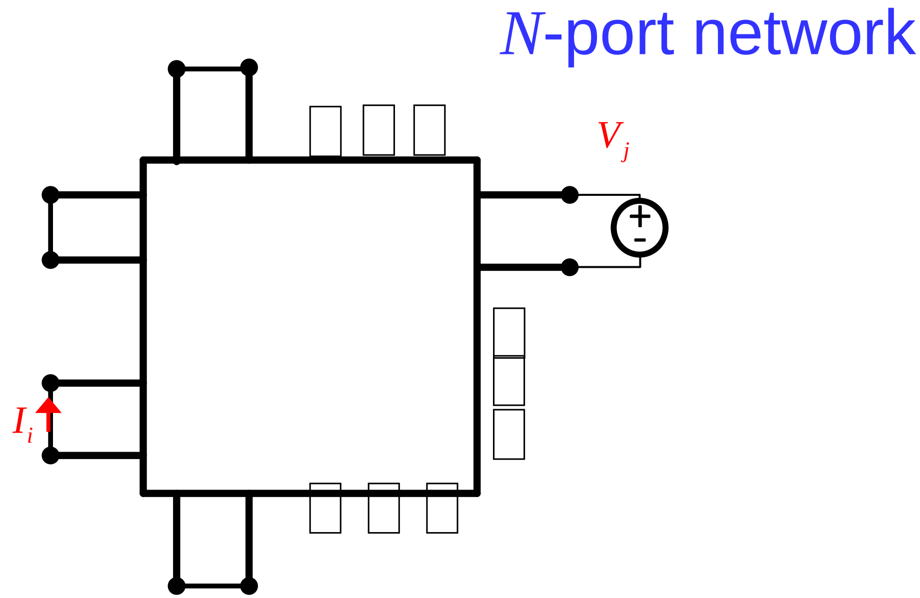
$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} \Rightarrow [I] = [Y][V]$$

$$\boxed{Y_{ij} = \left.\frac{I_i}{V_j}\right|_{V_k=0 \quad k \neq j}}$$

Short-circuit parameters

Y-Parameters (cont.)

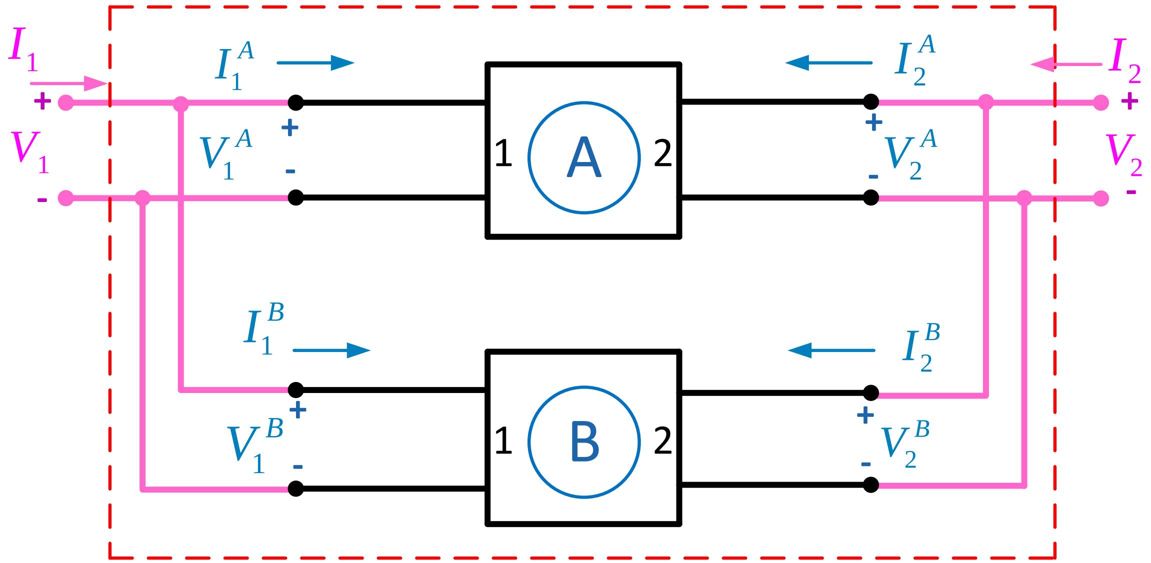
$$Y_{ij} = \left.\frac{I_i}{V_j}\right|_{V_k=0 \quad k \neq j}$$



We apply a voltage across port j and measure the current (with an ideal current meter) at port i. All ports are short-circuited except j.

Y-Parameters (cont.)

Y-parameters are convenient for parallel connected networks.



Parallel:

$$V_1 = V_1^A = V_1^B$$

$$V_2 = V_2^A = V_2^B$$

$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} I_1^A \\ I_2^A \end{bmatrix} + \begin{bmatrix} I_1^B \\ I_2^B \end{bmatrix} = \begin{bmatrix} Y_{11}^A & Y_{12}^A \\ Y_{21}^A & Y_{22}^A \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} + \begin{bmatrix} Y_{11}^B & Y_{12}^B \\ Y_{21}^B & Y_{22}^B \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11}^A + Y_{11}^B & Y_{12}^A + Y_{12}^B \\ Y_{21}^A + Y_{21}^B & Y_{22}^A + Y_{22}^B \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

Relation Between Z and Y Parameters

Relation between [Z] and [Y] matrices:

$$[V] = [Z][I]$$

$$[I] = [Y][V]$$

Hence:

$$\begin{aligned}[V] &= [Z]\big([Y][V]\big)\\ &= \big([Z][Y]\big)[V]\end{aligned}$$

It follows that

$$[Z][Y] = [U] = \text{Identity Matrix}$$

Therefore $$\boxed{[Y] = [Z]^{-1}}$$

Reciprocal Networks

If a network does not contain non-reciprocal devices or materials* (i.e. ferrites, or active devices), then the network is "reciprocal."

$$\Rightarrow Z_{ij} = Z_{ji} \quad \left(Y_{ij} = Y_{ji} \right)$$

Note: The inverse of a symmetric matrix is symmetric.

$[Z]$ and $[Y]$ are symmetric matrices

* A reciprocal material is one that has symmetric permittivity and permeability tensors. A reciprocal device is one that is made from reciprocal materials.

Example of a nonreciprocal material: a biased ferrite

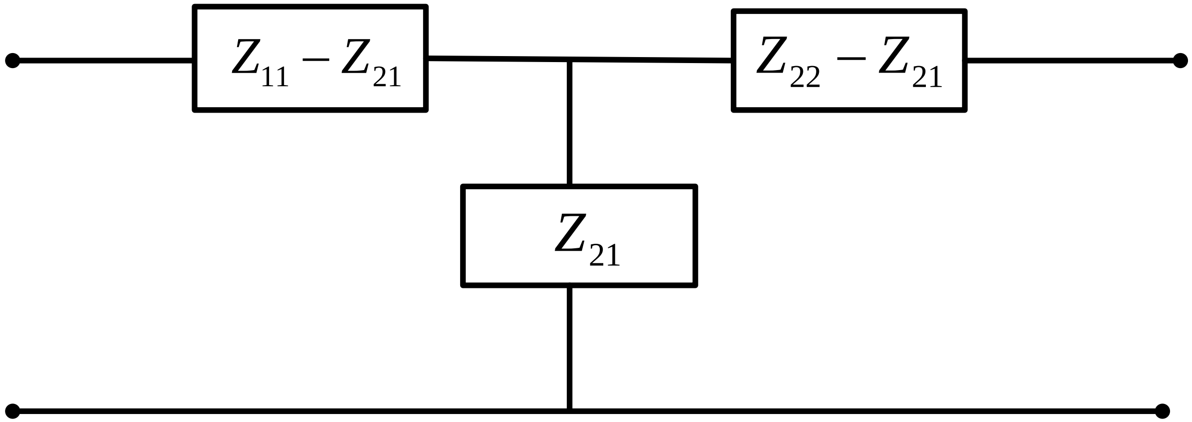
(This is very useful for making isolators and circulators.)

Reciprocal Networks (cont.)

We can show that the equivalent circuits for reciprocal 2-port networks are:

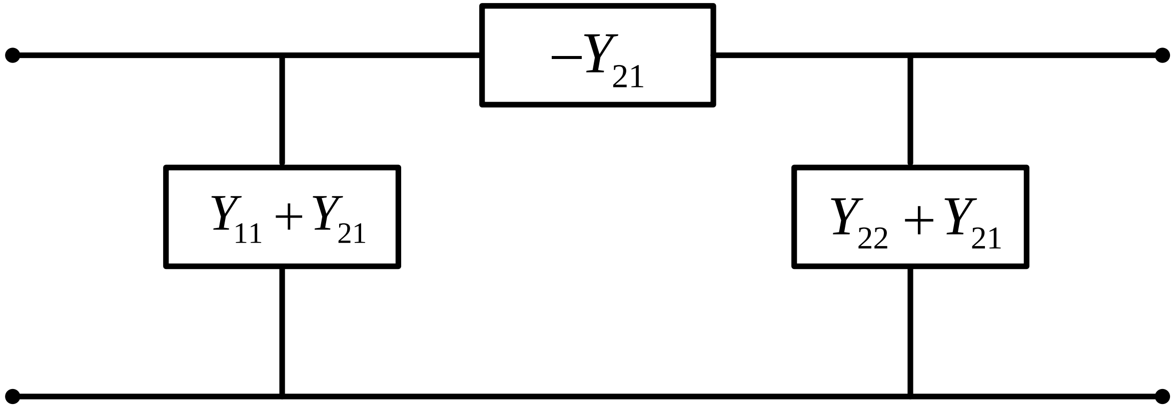
T-equivalent

"T network"



Pi-equivalent

"Π network"



ABCD-Parameters

They are defined only for <u>2-port</u> networks.

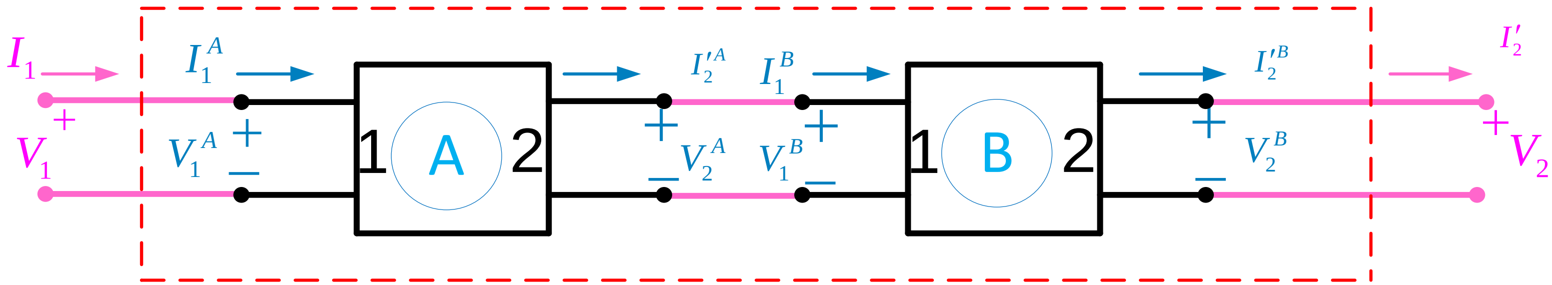
$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ I_2' \end{bmatrix}$$

$$I_2' = -I_2$$

$$A = \left.\frac{V_1}{V_2}\right|_{I_2'=0} \qquad C = \left.\frac{I_1}{V_2}\right|_{I_2'=0}$$

$$B = \left.\frac{V_1}{I_2'}\right|_{V_2=0} \qquad D = \left.\frac{I_1}{I_2'}\right|_{V_2=0}$$

Cascaded Networks



$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} V_1^A \\ I_1^A \end{bmatrix} = \left[ABCD^A \right] \begin{bmatrix} V_2^A \\ I_2'^A \end{bmatrix}$$

$$= \left[ABCD^A \right] \begin{bmatrix} V_1^B \\ I_1^B \end{bmatrix}$$

$$= \underbrace{\left[ABCD^A \right] \left[ABCD^B \right]} \begin{bmatrix} V_2^B \\ I_2'^B \end{bmatrix}$$

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \left[ABCD^{AB} \right] \begin{bmatrix} V_2 \\ I_2' \end{bmatrix}$$

A nice property of the ABCD matrix is that it is easy to use with cascaded networks: you simply multiply the ABCD matrices together.

Scattering Parameters

Problems to use Z- or Y-matrix in microwave circuits

- ❑ difficult in defining voltage and current for non-TEM lines
- ❑ no equipment available to measure voltage and current in complex value

  (eg. sampling scope in microwave range, impedance meter <3GHz)
- ❑ difficult to make open and short circuits over broadband
- ❑ active devices not stable as terminated with open or short circuit

Scattering Parameters

- At high frequencies, Z, Y, & $ABCD$ parameters are difficult (if not impossible) to measure.

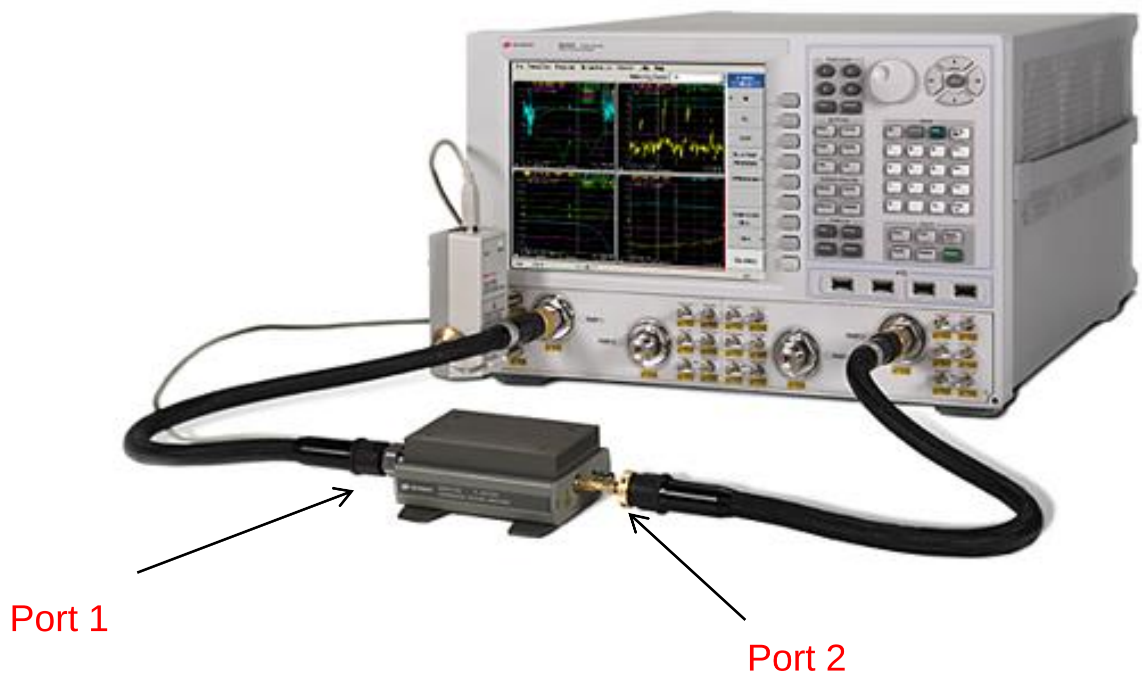
  - V and I are not always uniquely defined (e.g., microstrip, waveguides).
  - Even if defined, V and I are extremely difficult to measure (particularly I).
  - Required open and short-circuit conditions are often difficult to achieve.

- Scattering (S) parameters are often the best representation for multi-port networks at high frequency.

Note: We can always convert from S parameters to Z, Y, or $ABCD$ parameters.

Scattering Parameters (cont.)

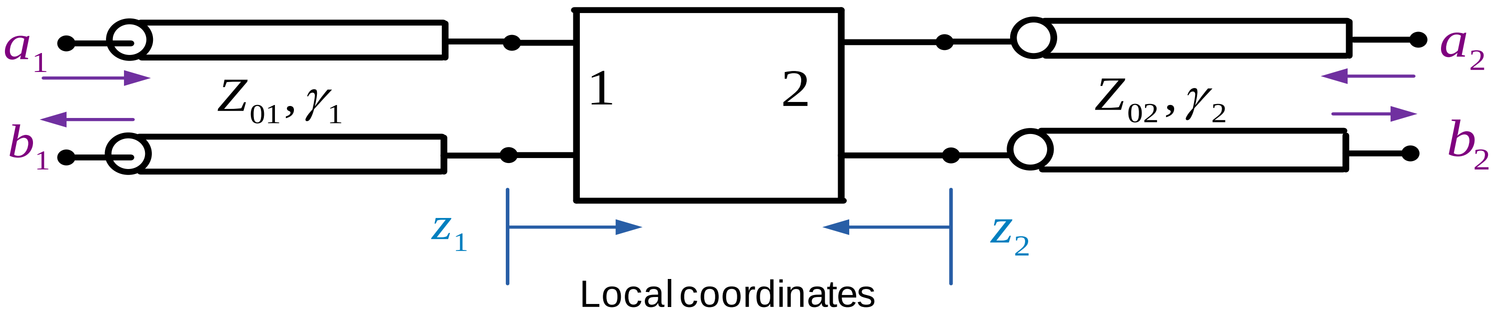
A Vector Network Analyzer (VNA) is usually used to measure S parameters.



Keysight (formerly Agilent) VNA shown performing a measurement.

Scattering Parameters (cont.)

S-parameters are defined
assuming transmission lines are connected to each port.



On each transmission line:

$$V_i(z_i) = V_{i0}^{+} e^{-\gamma_i z_i} + V_{i0}^{-} e^{+\gamma_i z_i} = V_i^{+}(z_i) + V_i^{-}(z_i)$$

$$I_i(z_i) = \frac{V_i^{+}(z_i)}{Z_{0i}} - \frac{V_i^{-}(z_i)}{Z_{0i}} \qquad i = 1,\, 2$$

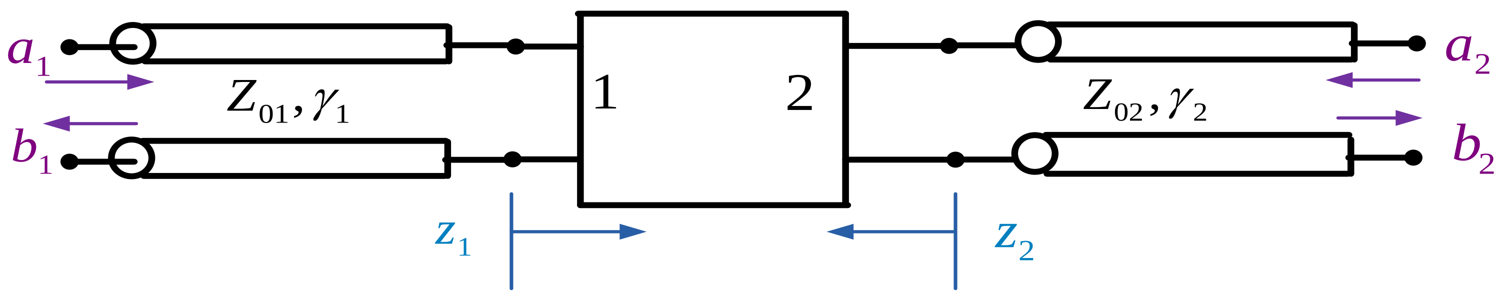
We define:

Incoming wave function $\equiv a_i(z_i) \equiv V_i^{+}(z_i) \big/ \sqrt{Z_{0i}}$

Outgoing wave function $\equiv b_i(z_i) \equiv V_i^{-}(z_i) \big/ \sqrt{Z_{0i}}$

Scattering Parameters (cont.)

Why are the wave functions (a and b) defined as they are?



$$P_i^+(0) = \frac{1}{2}\operatorname{Re}\left[V_i^+(0)\, I_i^{+^*}(0)\right] = \frac{1}{2}\frac{\left|V_i^+(0)\right|^2}{Z_{0i}}$$

(assuming lossless lines)

Recall: $a_i(0) \equiv V_i^+(0) \big/ \sqrt{Z_{0i}}$

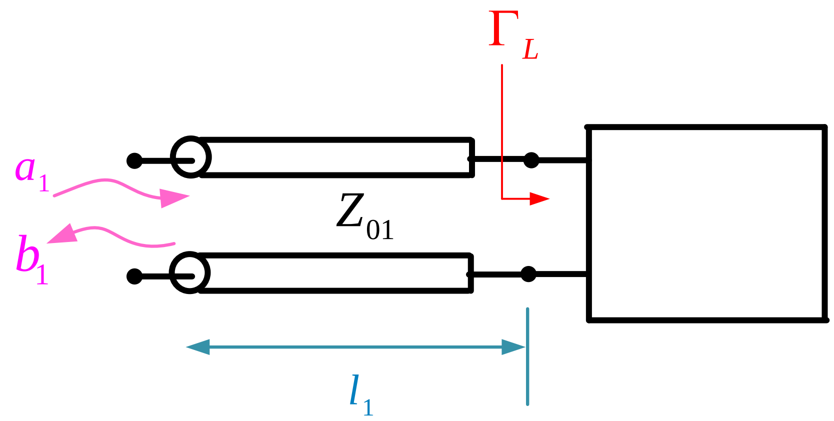
$$\Rightarrow\ P_i^+(0) = \frac{1}{2}\left|a_i(0)\right|^2$$

Similarly,

$$P_i^-(0) = \frac{1}{2}\frac{\left|V_i^-(0)\right|^2}{Z_{0i}} = \frac{1}{2}\left|b_i(0)\right|^2$$

For a One-Port Network

$$\Gamma_L = \frac{V_1^-(0)}{V_1^+(0)} = \frac{V_1^-(0)\big/\sqrt{Z_{01}}}{V_1^+(0)\big/\sqrt{Z_{01}}} = \frac{b_1(0)}{a_1(0)}$$



$$S_{11} \equiv \frac{b_1(0)}{a_1(0)}$$

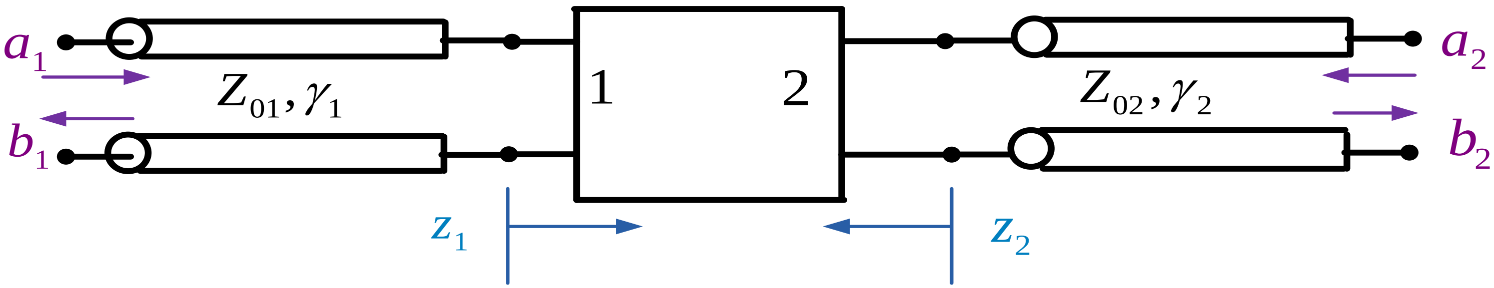
$$\Gamma_L = S_{11}$$

For a one-port network, S_{11} is the same as Γ_L.

Incoming wave function $\equiv a_i(z_i) \equiv V_i^+(z_i)\big/\sqrt{Z_{0i}}$

Outgoing wave function $\equiv b_i(z_i) \equiv V_i^-(z_i)\big/\sqrt{Z_{0i}}$

For a Two-Port Network



From linearity:

$$b_1(0) = S_{11}a_1(0) + S_{12}a_2(0)$$
$$b_2(0) = S_{21}a_1(0) + S_{22}a_2(0)$$

Scattering matrix

$$\Rightarrow \begin{bmatrix} b_1(0) \\ b_2(0) \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \begin{bmatrix} a_1(0) \\ a_2(0) \end{bmatrix} \Rightarrow [b] = [S][a]$$

Scattering Parameters

$$b_1(0) = S_{11}a_1(0) + S_{12}a_2(0)$$
$$b_2(0) = S_{21}a_1(0) + S_{22}a_2(0)$$

$$S_{11} = \left.\frac{b_1(0)}{a_1(0)}\right|_{a_2=0}$$ Output is matched ← input reflection coef. w/ output matched

$$S_{12} = \left.\frac{b_1(0)}{a_2(0)}\right|_{a_1=0}$$ Input is matched ← reverse transmission coef. w/ input matched

$$S_{21} = \left.\frac{b_2(0)}{a_1(0)}\right|_{a_2=0}$$ Output is matched ← forward transmission coef. w/ output matched

$$S_{22} = \left.\frac{b_2(0)}{a_2(0)}\right|_{a_1=0}$$ Input is matched ← output reflection coef. w/ input matched

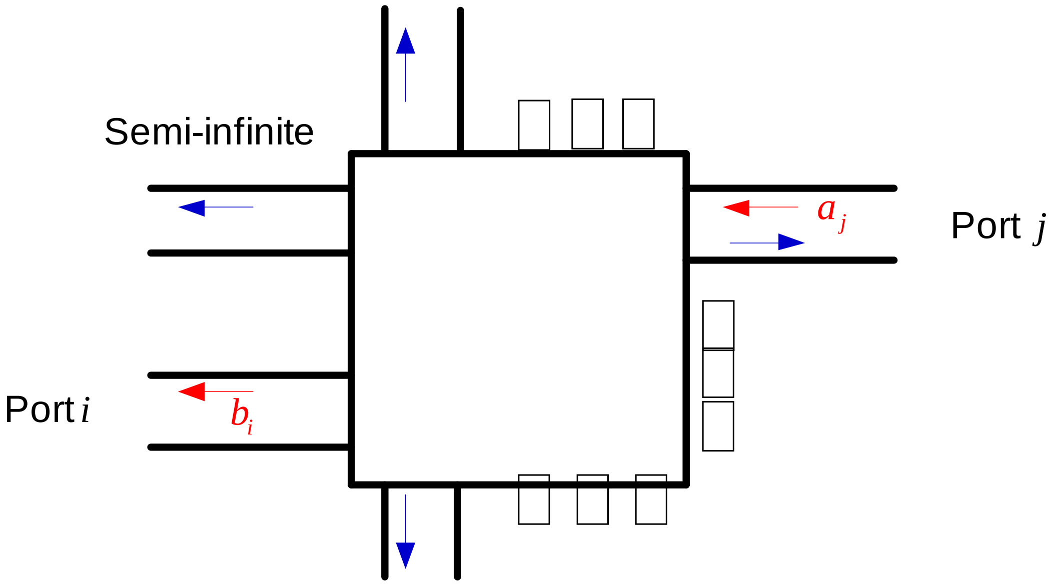
Scattering Parameters (cont.)

For a general multiport network:

$$S_{ij} = \left. \frac{b_i(0)}{a_j(0)} \right|_{a_k=0 \;\; k\neq j}$$

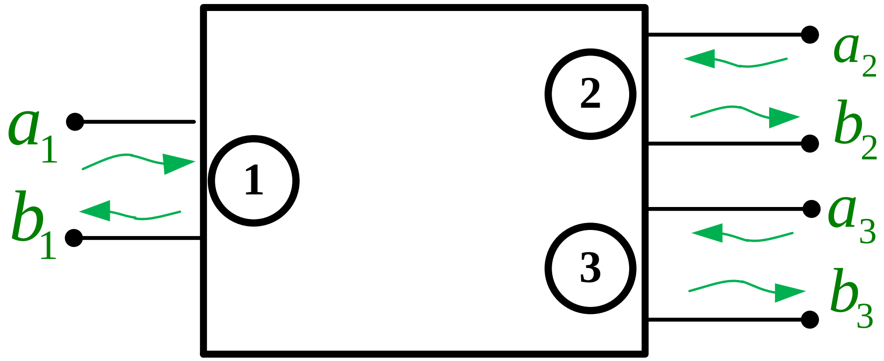
All ports except j are semi-infinite with no incident wave (or with matched load at ports).

N-port network



Scattering Parameters (cont.)

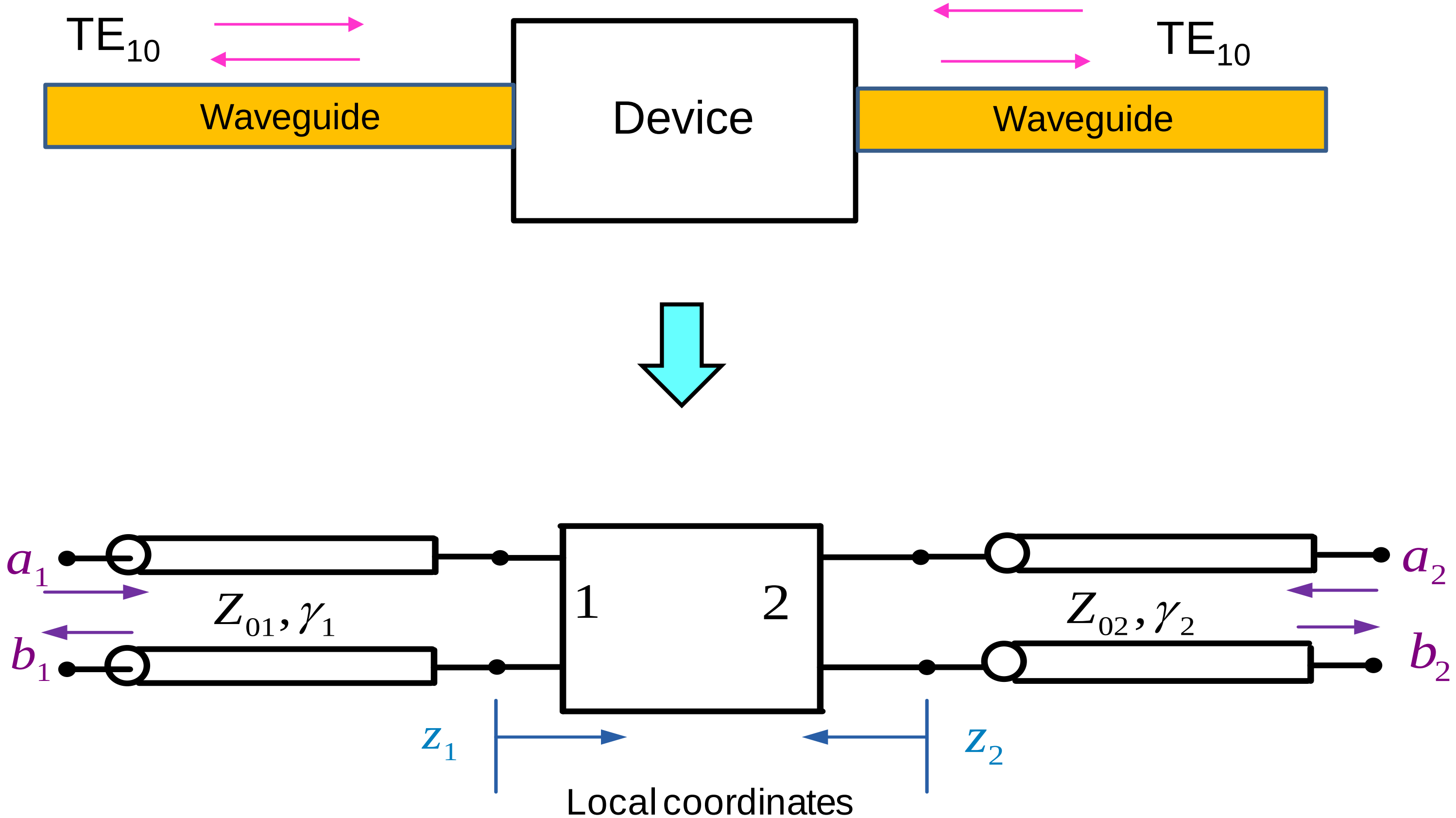
Illustration of a three-port network



$$b_1(0) = S_{11}a_1(0) + S_{12}a_2(0) + S_{13}a_3(0)$$
$$b_2(0) = S_{21}a_1(0) + S_{22}a_2(0) + S_{23}a_3(0)$$
$$b_3(0) = S_{31}a_1(0) + S_{23}a_2(0) + S_{33}a_3(0)$$

Scattering Parameters (cont.)

A microwave system may have waveguides entering a device. In this case, the transmission lines are TEN models for the waveguides.



Properties of the *S* Matrix

For reciprocal networks, the *S*-matrix is symmetric.

$$S_{ij} = S_{ji} \qquad i \neq j$$

$$\Rightarrow \quad [S] = [S]^T$$

Example of a nonreciprocal material: a biased ferrite

Properties of the S Matrix (cont.)

❖For lossless networks, the S-matrix is unitary.

$$\Rightarrow [S]^T [S]^* = [S]^* [S]^T = [U]$$

Identity matrix

Note :

If $[A][B] = [U]$

then

$[B][A] = [U]$

Equivalently,

$$[S]^{T*} = [S]^{-1}$$

Notation:

$$[S]^\dagger = [S]^H = [S]^{T*}$$

("Hermetian conjugate" or "Hermetian transpose")

so $[S]^\dagger = [S]^{-1}$

N-port network

Take (i, j) element $\Rightarrow \sum_{k=1}^{N} S_{ik}^T \; S_{kj}^* = \sum_{k=1}^{N} S_{ki} \; S_{kj}^* = \delta_{ij}$

$$\delta_{ij} = \begin{cases} 1\,;\; i = j \\ 0\,;\; i \neq j \end{cases}$$

Properties of the S Matrix (cont.)

$$\sum_{k=1}^{N} S_{ki}\, S_{kj}^{*} = \delta_{ij}$$

Interpretation: The inner product of columns i and j is zero unless $i = j$.

$$[S] = \begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{21} & S_{22} & S_{23} \\ S_{31} & S_{23} & S_{33} \end{bmatrix}$$

$\underline{S}_1$ vector

$\underline{S}_3$ vector

The rows also form orthogonal sets (see the note on the previous slide).

$$\underline{S}_i \cdot \underline{S}_j^{*} = \delta_{ij}$$

Scattering Parameters (cont.)

Note: If all lines entering the network have the same characteristic impedance, then

$$S_{ij} = \frac{b_i(0)}{a_j(0)} = \left.\frac{V_i^-(0)}{V_j^+(0)}\right|_{V_k^+=0\;\; k\neq j}$$

In general:

$$S_{ij} \equiv \left.\frac{V_i^-(0)}{V_j^+(0)}\right|_{V_k^+=0\;\; k\neq j}$$

"unnormalized" scattering parameters

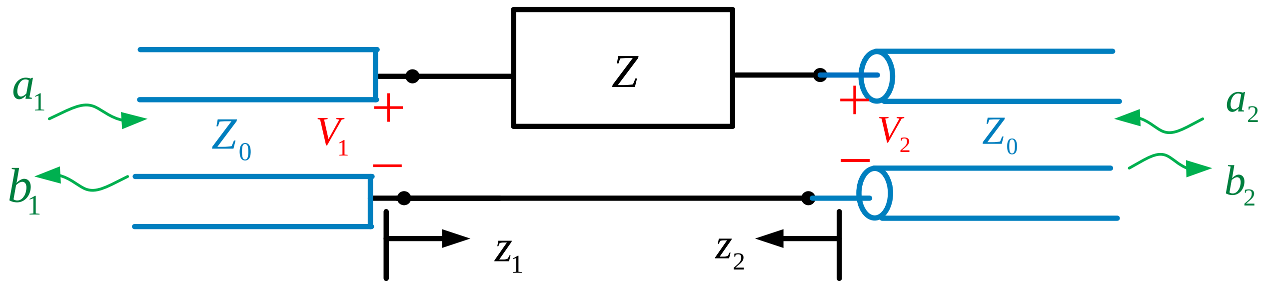
$$S_{ij} \equiv \left.\frac{b_i(0)}{a_j(0)}\right|_{a_k=0\;\; k\neq j}$$

"normalized" scattering parameters

Note: The unitary property of the scattering matrix requires normalized parameters.
We use normalized parameters in these notes.

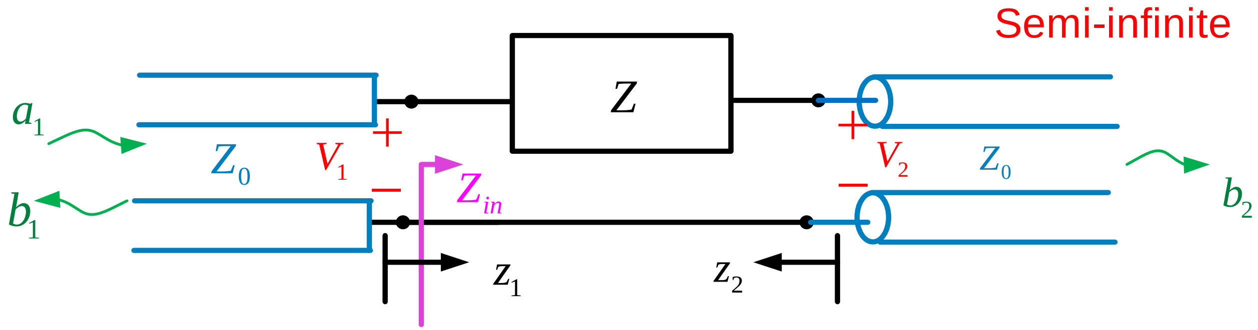
Example

Find the S parameters for a series impedance Z.



Note that two different coordinate systems are being used here!

Example (cont.)



S_{11} Calculation:

$$S_{11} = \left.\frac{b_1(0)}{a_1(0)}\right|_{a_2=0} = \frac{V_1^-(0)}{V_1^+(0)} = \left.\frac{Z_{in} - Z_0}{Z_{in} + Z_0}\right|_{a_2=0} = \frac{(Z + Z_0) - Z_0}{(Z + Z_0) + Z_0}$$

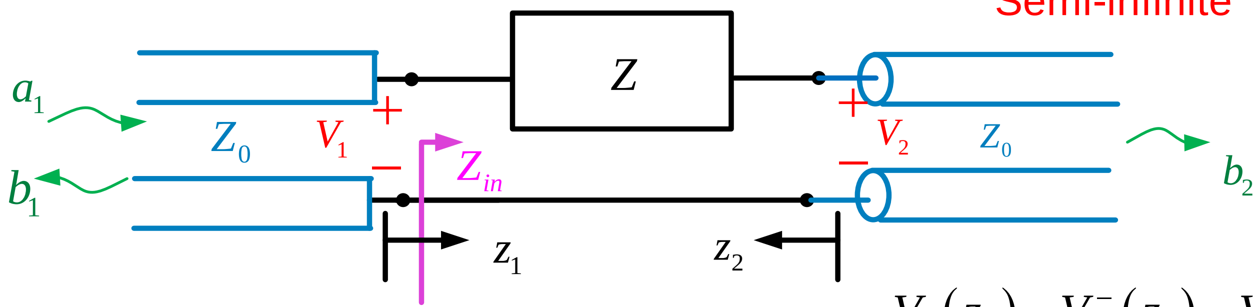
$$\Rightarrow \quad S_{11} = \frac{Z}{Z + 2Z_0}$$

By symmetry:

$$S_{22} = S_{11}$$

Example (cont.)

S_{21} Calculation:



$$V_2(z_2) = V_2^-(z_2) = V_2^-(0)e^{+jk_{z2}z_2}$$

$$S_{21} = \left.\frac{b_2(0)}{a_1(0)}\right|_{a_2=0}$$

$$= \left.\frac{V_2^-(0)}{V_1^+(0)}\right|_{a_2=0}$$

Note :

$$V_2^-(0) = b_2(0)\sqrt{Z_0}$$

$$V_1^+(0) = a_1(0)\sqrt{Z_0}$$

Voltage divider: $$V_2^-(0) = V_2(0) = V_1(0)\left(\frac{Z_0}{Z+Z_0}\right)$$

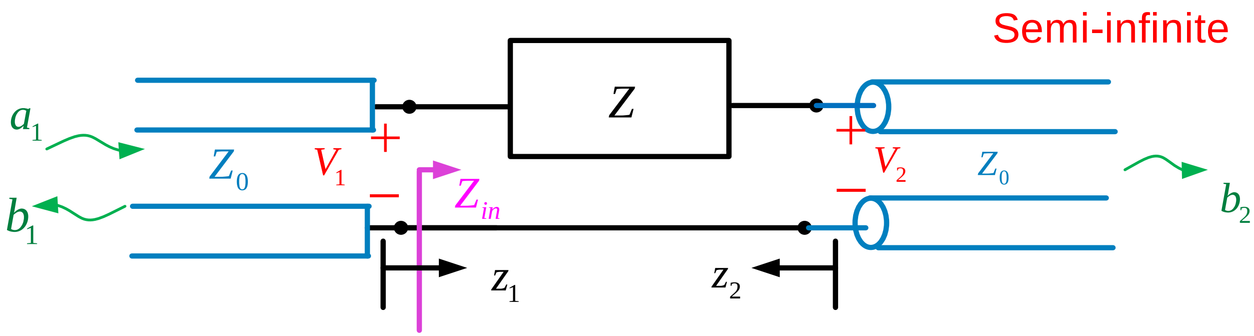
We also have

$$V_1(0) = V_1^+(0)(1+S_{11}) = a_1(0)\sqrt{Z_0}(1+S_{11})$$

so

$$V_2^-(0) = a_1(0)\sqrt{Z_0}(1+S_{11})\left(\frac{Z_0}{Z+Z_0}\right)$$

Example (cont.)



Hence

$$S_{21} = \frac{a_1(0)\sqrt{Z_0}\,(1+S_{11})\left(\dfrac{Z_0}{Z+Z_0}\right)}{a_1(0)\sqrt{Z_0}}$$

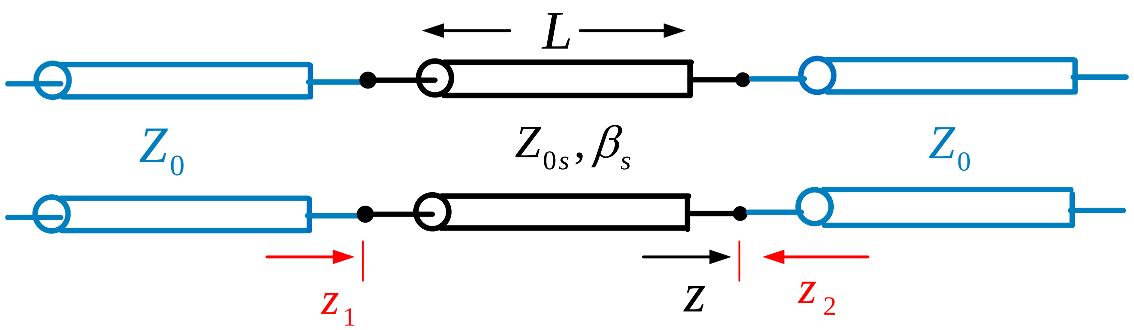
$$= (1+S_{11})\left(\frac{Z_0}{Z+Z_0}\right) = \left(1+\frac{Z}{Z+2Z_0}\right)\left(\frac{Z_0}{Z+Z_0}\right) = \left(\frac{2Z+2Z_0}{Z+2Z_0}\right)\left(\frac{Z_0}{Z+Z_0}\right)$$

We then have

$$\boxed{S_{21} = \frac{2\,Z_0}{Z+2\,Z_0}} \qquad \boxed{S_{12} = S_{21}}$$

Example

Find the S parameters for a length L of transmission line.

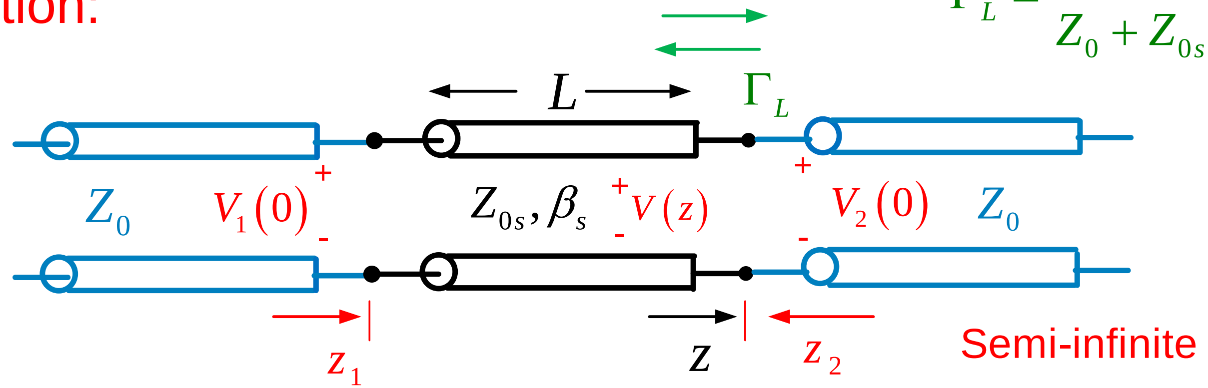


Note that three different coordinate systems are being used here!

Example (cont.)

S_{11} Calculation:

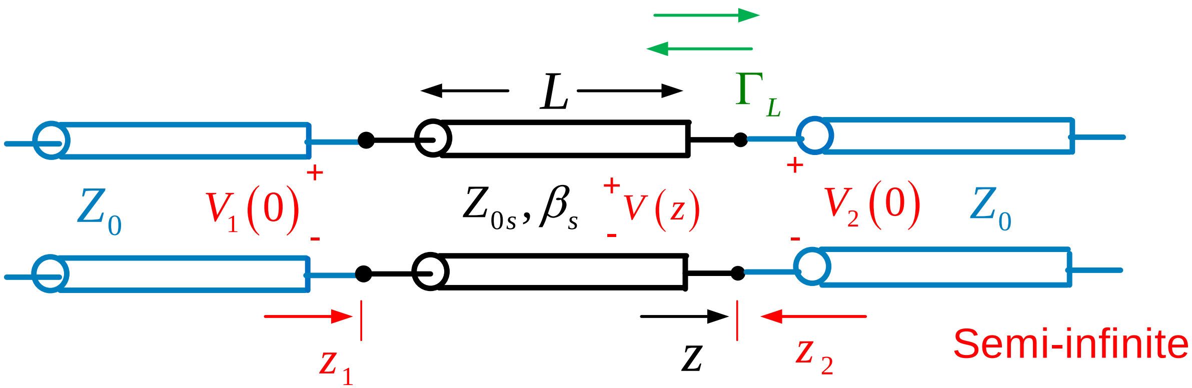
$$\Gamma_L = \frac{Z_0 - Z_{0s}}{Z_0 + Z_{0s}}$$



$$S_{11} = \left.\frac{b_1}{a_1}\right|_{a_2=0} = \frac{\left.Z_{in}\right|_{a_2=0} - Z_0}{\left.Z_{in}\right|_{a_2=0} + Z_0} = S_{22} \text{ (by symmetry)}$$

$$\left.Z_{in}\right|_{a_2=0} = Z_{0s}\frac{\left(Z_0 + jZ_{0s}\tan\beta_s L\right)}{\left(Z_{0s} + jZ_0\tan\beta_s L\right)} = Z_{0s}\frac{\left(1+\Gamma_L e^{-j2\beta_s L}\right)}{\left(1-\Gamma_L e^{-j2\beta_s L}\right)}$$

Example (cont.)



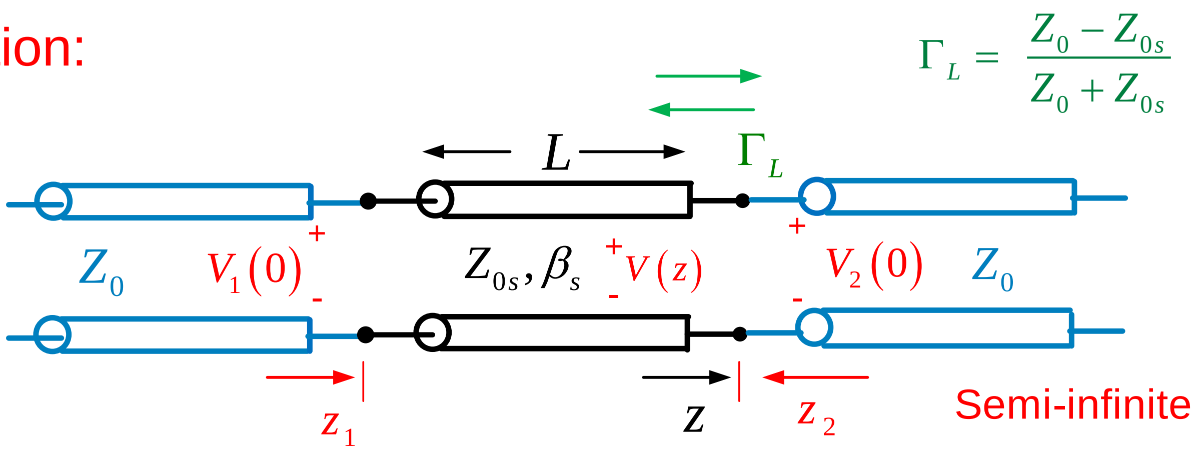
Hence

$$S_{11} = S_{22} = \frac{Z_{0s}\dfrac{\left(Z_0 + jZ_{0s}\tan\beta_s L\right)}{\left(Z_{0s} + jZ_0\tan\beta_s L\right)} - Z_0}{Z_{0s}\dfrac{\left(Z_0 + jZ_{0s}\tan\beta_s L\right)}{\left(Z_{0s} + jZ_0\tan\beta_s L\right)} + Z_0}$$

Note: If $Z_{0s} = Z_0 \Rightarrow \left. Z_{in}\right|_{a_2=0} = Z_0 \Rightarrow S_{11} = S_{22} = 0$

Example (cont.)

S_{21} Calculation:



$$S_{21} = \left.\frac{b_2}{a_1}\right|_{a_2=0} = \left.\frac{V_2^-(0)\big/\sqrt{Z_0}}{V_1^+(0)\big/\sqrt{Z_0}}\right|_{a_2=0}$$

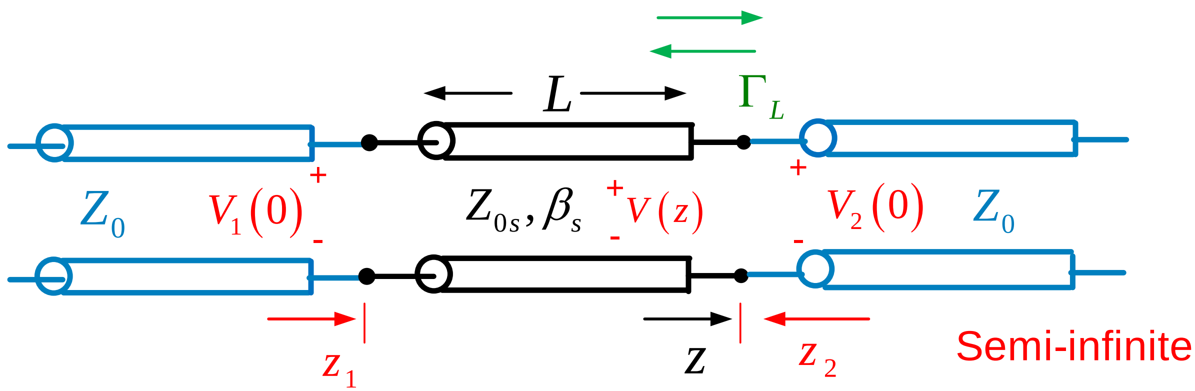
Total voltage at port 1: $V_1(0) = V_1^+(0)\left(1+S_{11}\right)$

Hence, for the denominator of the S_{21} equation we have

$$V_1^+(0) = \frac{V_1(0)}{1+S_{11}}$$

We now try to put the numerator of the S_{21} equation in terms of $V_1(0)$.

Example (cont.)



$$V_2^-(0) = V_2(0) = V(0) = V^+(0)(1+\Gamma_L)$$

Next, we need to get $V^+(0)$ in terms of $V_1(0)$:

$$V(z) = V^+(0)e^{-j\beta_s z}\left(1+\Gamma_L e^{+j2\beta_s z}\right)$$

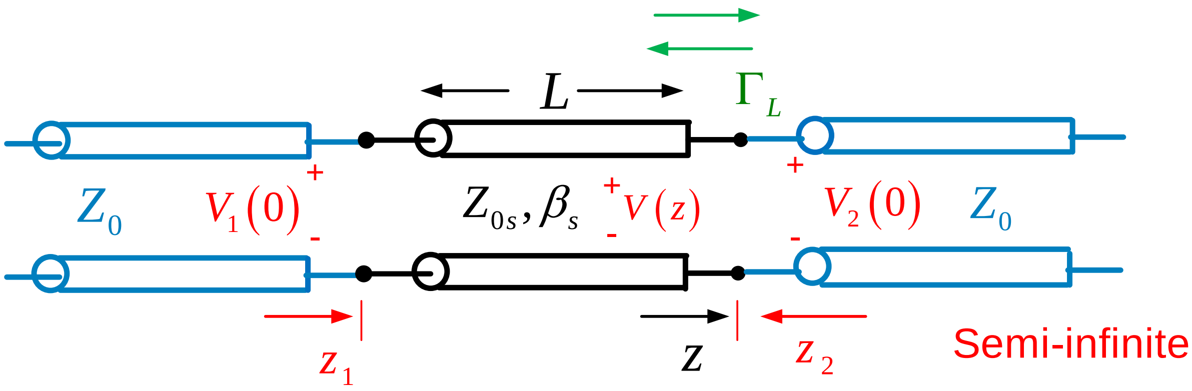
$$\Rightarrow V_1(0) = V(-L) = V^+(0)e^{+j\beta_s L}\left(1+\Gamma_L e^{-j2\beta_s L}\right)$$

$$\Rightarrow V^+(0) = \frac{V_1(0)}{e^{+j\beta_s L}\left(1+\Gamma_L e^{-j2\beta_s L}\right)}$$

Hence, we have

$$V_2^-(0) = \frac{V_1(0)}{e^{+j\beta_s L}\left(1+\Gamma_L e^{-j2\beta_s L}\right)}(1+\Gamma_L)$$

Example (cont.)



$$V_2^-(0) = \frac{V_1(0)}{e^{+j\beta_s L}\left(1+\Gamma_L e^{-j2\beta_s L}\right)}\left(1+\Gamma_L\right)$$

$$V_1^+(0) = \frac{V_1(0)}{1+S_{11}}$$

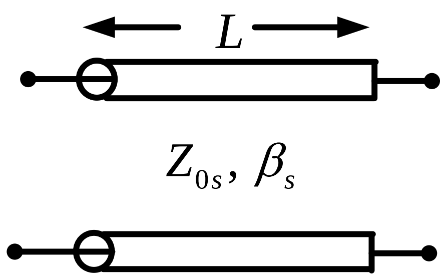
Therefore, we have

$$S_{21} = \left.\frac{V_2^-(0)}{V_1^+(0)}\right|_{a_2=0} = \frac{\left(1+S_{11}\right)\left(1+\Gamma_L\right)e^{-j\beta_s L}}{1+\Gamma_L e^{-j2\beta_s L}}$$

so

$$S_{21} = \frac{\left(1+S_{11}\right)\left(1+\Gamma_L\right)e^{-j\beta_s L}}{1+\Gamma_L e^{-j2\beta_s L}} = S_{12} \text{ by symmetry}$$

Example (cont.)



Special cases:

$$a)\quad Z_{0s} = Z_0$$

$$Z_{0s} = Z_0 \Rightarrow S_{11} = S_{22} = 0, \quad \Gamma_L = 0$$

$$S_{21} = S_{12} = e^{-j\beta_s L}$$

$$a) \quad [S] = \begin{bmatrix} 0 & e^{-j\beta_s L} \\ e^{-j\beta_s L} & 0 \end{bmatrix}$$

$$b)\quad L = \frac{\lambda_g}{2}$$

$$L = \frac{\lambda_g}{2} \Rightarrow \beta_s L = \frac{2\pi}{\lambda_g}\frac{\lambda_g}{2} = \pi$$

$$\Rightarrow Z_{in}\big|_{a_2=0} = Z_0 \quad \Rightarrow S_{11} = S_{22} = 0$$

$$e^{-j\beta_s L} = -1, \quad e^{-j2\beta_s L} = +1 \quad \Rightarrow \quad S_{21} = -1$$

$$b) \quad [S] = \begin{bmatrix} 0 & -1 \\ -1 & 0 \end{bmatrix}$$

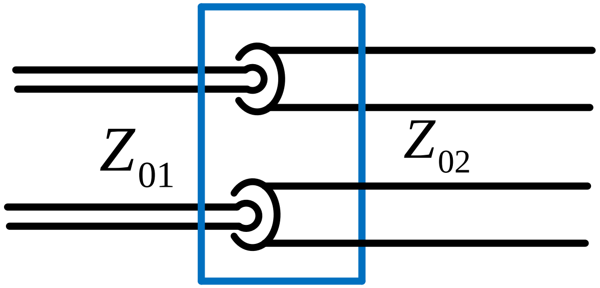
Example

Find the S parameters for a step-impedance discontinuity.

S_{11} Calculation:

$$S_{11} = \frac{Z_{02} - Z_{01}}{Z_{02} + Z_{01}}$$

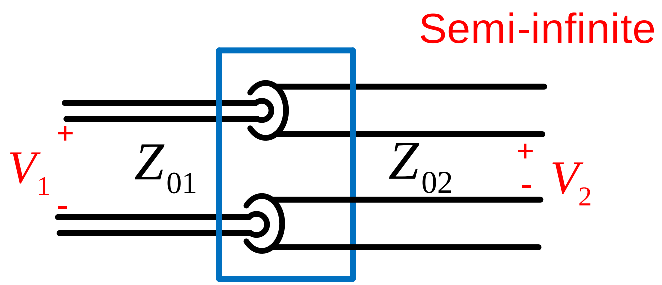
$$S_{22} = \frac{Z_{01} - Z_{02}}{Z_{02} + Z_{01}} = -S_{11}$$



S_{21} Calculation:

$$S_{21} = \left.\frac{b_2(0)}{a_1(0)}\right|_{a_2=0} = \left.\frac{\dfrac{V_2^-(0)}{\sqrt{Z_{02}}}}{\dfrac{V_1^+(0)}{\sqrt{Z_{01}}}}\right|_{a_2=0}$$

Example (cont.)



Because of continuity of the voltage across the junction, we have:

$$V_2^-(0)\Big|_{a_2=0} = V_2(0)\Big|_{a_2=0} = V_1(0)\Big|_{a_2=0} = V_1^+(0)\left(1+S_{11}\right)$$

$$S_{21} = \left.\frac{\dfrac{V_2^-(0)}{\sqrt{Z_{02}}}}{\dfrac{V_1^+(0)}{\sqrt{Z_{01}}}}\right|_{a_2=0} = \left.\frac{\dfrac{V_1^+(0)\left(1+S_{11}\right)}{\sqrt{Z_{02}}}}{\dfrac{V_1^+(0)}{\sqrt{Z_{01}}}}\right|_{a_2=0}$$

$$1+S_{11} = 1+\frac{Z_{02}-Z_{01}}{Z_{02}+Z_{01}}$$
$$= \frac{2Z_{02}}{Z_{02}+Z_{01}}$$

so

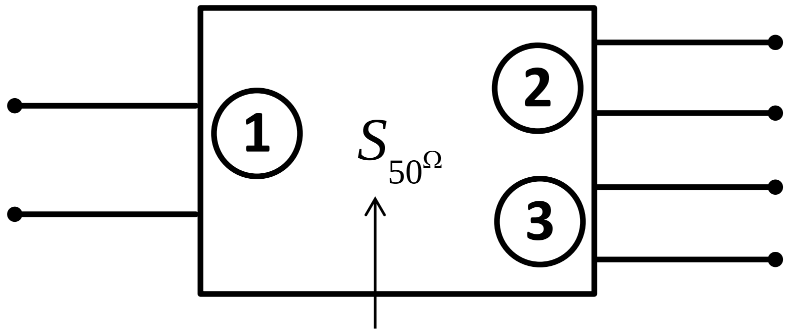
$$S_{21} = \left(1+S_{11}\right)\sqrt{\frac{Z_{01}}{Z_{02}}}$$

Hence

$$S_{21} = S_{12} = 2\frac{\sqrt{Z_{01}Z_{02}}}{Z_{01}+Z_{02}}$$

Example

$$\left[S_{50\Omega}\right] = \begin{bmatrix} 0 & \dfrac{-j}{\sqrt{2}} & \dfrac{-j}{\sqrt{2}} \\ \dfrac{-j}{\sqrt{2}} & 0 & 0 \\ \dfrac{-j}{\sqrt{2}} & 0 & 0 \end{bmatrix}$$



These are the S parameters assuming 50 Ω lines entering the device.

Not unitary $\rightarrow$ Not lossless

(For example, column 2 doted with the conjugate of column 3 is not zero.)

1) Find the input impedance looking into port 1 when ports 2 and 3 are terminated in 50 [Ω] loads.

2) Find the input impedance looking into port 1 when port 2 is terminated in a 75 [Ω] load and port 3 is terminated in a 50 [Ω] load.

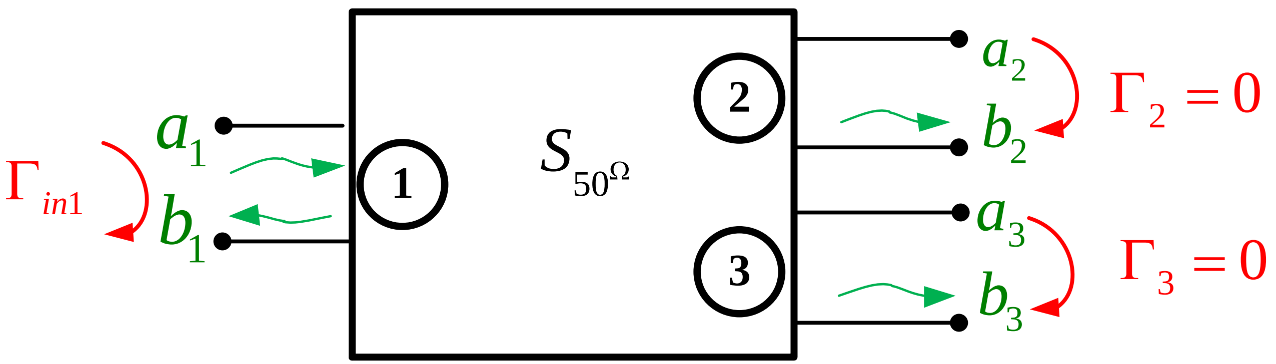
Example (cont.)

1) If ports 2 and 3 are terminated in 50 [Ω]: $(a_2 = a_3 = 0)$

$$b_1 = S_{11}a_1 + S_{12}\cancel{a_2} + S_{13}\cancel{a_3}$$

$$\Rightarrow \Gamma_{in1} = \frac{b_1}{a_1} = S_{11} = 0 \quad \Rightarrow \quad Z_{in1} = Z_{01}$$

$$\Rightarrow \quad \boxed{Z_{in1} = 50[\Omega]}$$

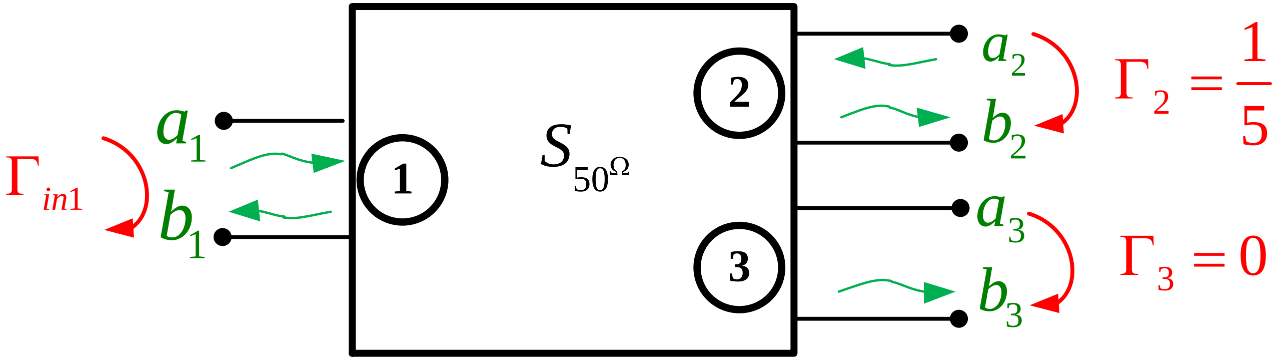


Example (cont.)

2) If port 2 is terminated in 75 [Ω] and port 3 in 50 [Ω]:

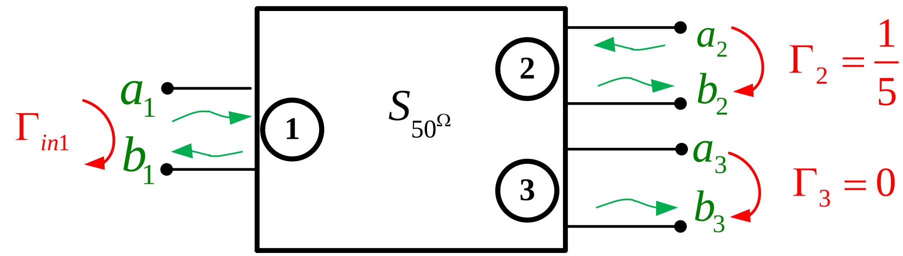
$$\Gamma_2 = \frac{a_2}{b_2} = \frac{75-50}{75+50} = \frac{1}{5}$$

$$\Gamma_3 = \frac{a_3}{b_3} = \frac{50-50}{50+50} = 0$$



Example (cont.)

$$\begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix} = \begin{bmatrix} 0 & \frac{-j}{\sqrt{2}} & \frac{-j}{\sqrt{2}} \\ \frac{-j}{\sqrt{2}} & 0 & 0 \\ \frac{-j}{\sqrt{2}} & 0 & 0 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}$$



$$b_2 / a_1 = S_{21} + \cancel{S_{22}\left(\frac{a_2}{a_1}\right)} + \cancel{S_{23}\left(\frac{a_3}{a_1}\right)}$$

$$\Rightarrow \Gamma_{in1} = \frac{b_1}{a_1} = \cancel{S_{11}} + S_{12}\frac{a_2}{a_1} + \cancel{S_{13}\frac{a_3}{a_1}}$$

$$= S_{12}\left(\frac{\Gamma_2 b_2}{a_1}\right) = S_{12}\left(\Gamma_2 S_{21}\right) = \left(\frac{-j}{\sqrt{2}}\right)\left(\frac{1}{5}\right)\left(\frac{-j}{\sqrt{2}}\right) = -\frac{1}{10}$$

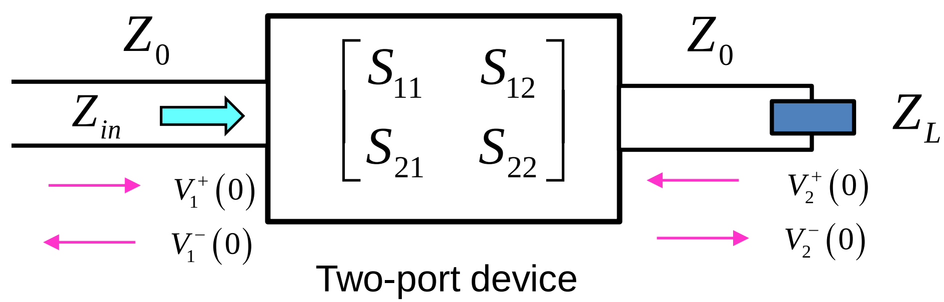
$$a_2 = \Gamma_2 b_2$$

$$\boxed{Z_{in1} = 50\left(\frac{1+\Gamma_{in_1}}{1-\Gamma_{in_1}}\right) = 44.55[\Omega]}$$

Example

Find Γ_{in} for the system shown below.

$$\Gamma_{in} = \frac{Z_{in} - Z_0}{Z_{in} + Z_0}$$



$$\Gamma_L = \frac{Z_L - Z_0}{Z_L - Z_0}$$

Assume : $V_1^+(0) = 1V$

so $\Gamma_{in} = V_1^-(0) = S_{11}(1) + S_{12}V_2^+(0)$

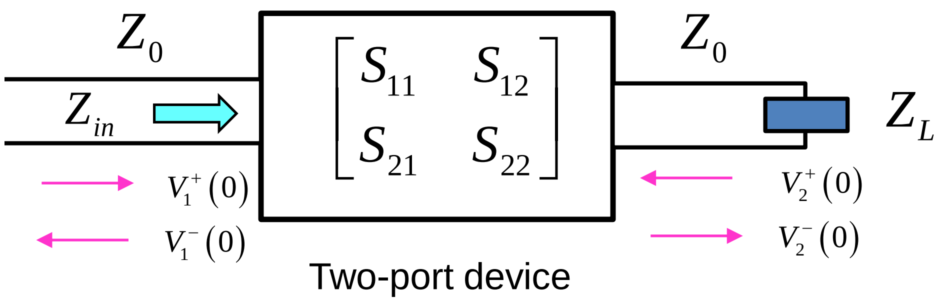
We also have:

$$\left.\begin{aligned} V_2^+(0) &= \Gamma_L V_2^-(0) \\ V_2^-(0) &= S_{21}(1) + S_{22}V_2^+(0) \end{aligned}\right\} \quad V_2^+(0) = \Gamma_L\left(S_{21}(1) + S_{22}V_2^+(0)\right)$$

$$\Downarrow$$

$$V_2^+(0) = \frac{\Gamma_L S_{21}}{1 - S_{22}\Gamma_L}$$

Example (cont.)



Hence

$$\begin{aligned}\Gamma_{in} &= S_{11} + S_{12} V_2^+(0) \\ &= S_{11} + S_{12}\left(\frac{\Gamma_L S_{21}}{1 - S_{22}\Gamma_L}\right)\end{aligned}$$

so

$$\boxed{\Gamma_{in} = S_{11} + \left(\frac{\Gamma_L S_{12} S_{21}}{1 - S_{22}\Gamma_L}\right)}$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L - Z_0}$$

Conversion Between Parameters
(Two-Ports)

TABLE 4.2 **Conversions Between Two-Port Network Parameters**

	S	Z	Y	$ABCD$
S_{11}	S_{11}	$\frac{(Z_{11}-Z_0)(Z_{22}+Z_0)-Z_{12}Z_{21}}{\Delta Z}$	$\frac{(Y_0-Y_{11})(Y_0+Y_{22})+Y_{12}Y_{21}}{\Delta Y}$	$\frac{A+B/Z_0-CZ_0-D}{A+B/Z_0+CZ_0+D}$
S_{12}	S_{12}	$\frac{2Z_{12}Z_0}{\Delta Z}$	$\frac{-2Y_{12}Y_0}{\Delta Y}$	$\frac{2(AD-BC)}{A+B/Z_0+CZ_0+D}$
S_{21}	S_{21}	$\frac{2Z_{21}Z_0}{\Delta Z}$	$\frac{-2Y_{21}Y_0}{\Delta Y}$	$\frac{2}{A+B/Z_0+CZ_0+D}$
S_{22}	S_{22}	$\frac{(Z_{11}+Z_0)(Z_{22}-Z_0)-Z_{12}Z_{21}}{\Delta Z}$	$\frac{(Y_0+Y_{11})(Y_0-Y_{22})+Y_{12}Y_{21}}{\Delta Y}$	$\frac{-A+B/Z_0-CZ_0+D}{A+B/Z_0+CZ_0+D}$
Z_{11}	$Z_0\frac{(1+S_{11})(1-S_{22})+S_{12}S_{21}}{(1-S_{11})(1-S_{22})-S_{12}S_{21}}$	Z_{11}	$\frac{Y_{22}}{\lvert Y\rvert}$	$\frac{A}{C}$
Z_{12}	$Z_0\frac{2S_{12}}{(1-S_{11})(1-S_{22})-S_{12}S_{21}}$	Z_{12}	$\frac{-Y_{12}}{\lvert Y\rvert}$	$\frac{AD-BC}{C}$
Z_{21}	$Z_0\frac{2S_{21}}{(1-S_{11})(1-S_{22})-S_{12}S_{21}}$	Z_{21}	$\frac{-Y_{21}}{\lvert Y\rvert}$	$\frac{1}{C}$
Z_{22}	$Z_0\frac{(1-S_{11})(1+S_{22})+S_{12}S_{21}}{(1-S_{11})(1-S_{22})-S_{12}S_{21}}$	Z_{22}	$\frac{Y_{11}}{\lvert Y\rvert}$	$\frac{D}{C}$
Y_{11}	$Y_0\frac{(1-S_{11})(1+S_{22})+S_{12}S_{21}}{(1+S_{11})(1+S_{22})-S_{12}S_{21}}$	$\frac{Z_{22}}{\lvert Z\rvert}$	Y_{11}	$\frac{D}{B}$
Y_{12}	$Y_0\frac{-2S_{12}}{(1+S_{11})(1+S_{22})-S_{12}S_{21}}$	$\frac{-Z_{12}}{\lvert Z\rvert}$	Y_{12}	$\frac{BC-AD}{B}$
Y_{21}	$Y_0\frac{-2S_{21}}{(1+S_{11})(1+S_{22})-S_{12}S_{21}}$	$\frac{-Z_{21}}{\lvert Z\rvert}$	Y_{21}	$\frac{-1}{B}$
Y_{22}	$Y_0\frac{(1+S_{11})(1-S_{22})+S_{12}S_{21}}{(1+S_{11})(1+S_{22})-S_{12}S_{21}}$	$\frac{Z_{11}}{\lvert Z\rvert}$	Y_{22}	$\frac{A}{B}$
A	$\frac{(1+S_{11})(1-S_{22})+S_{12}S_{21}}{2S_{21}}$	$\frac{Z_{11}}{Z_{21}}$	$\frac{-Y_{22}}{Y_{21}}$	A
B	$Z_0\frac{(1+S_{11})(1+S_{22})-S_{12}S_{21}}{2S_{21}}$	$\frac{\lvert Z\rvert}{Z_{21}}$	$\frac{-1}{Y_{21}}$	B
C	$\frac{1}{Z_0}\frac{(1-S_{11})(1-S_{22})-S_{12}S_{21}}{2S_{21}}$	$\frac{1}{Z_{21}}$	$\frac{-\lvert Y\rvert}{Y_{21}}$	C
D	$\frac{(1-S_{11})(1+S_{22})+S_{12}S_{21}}{2S_{21}}$	$\frac{Z_{22}}{Z_{21}}$	$\frac{-Y_{11}}{Y_{21}}$	D

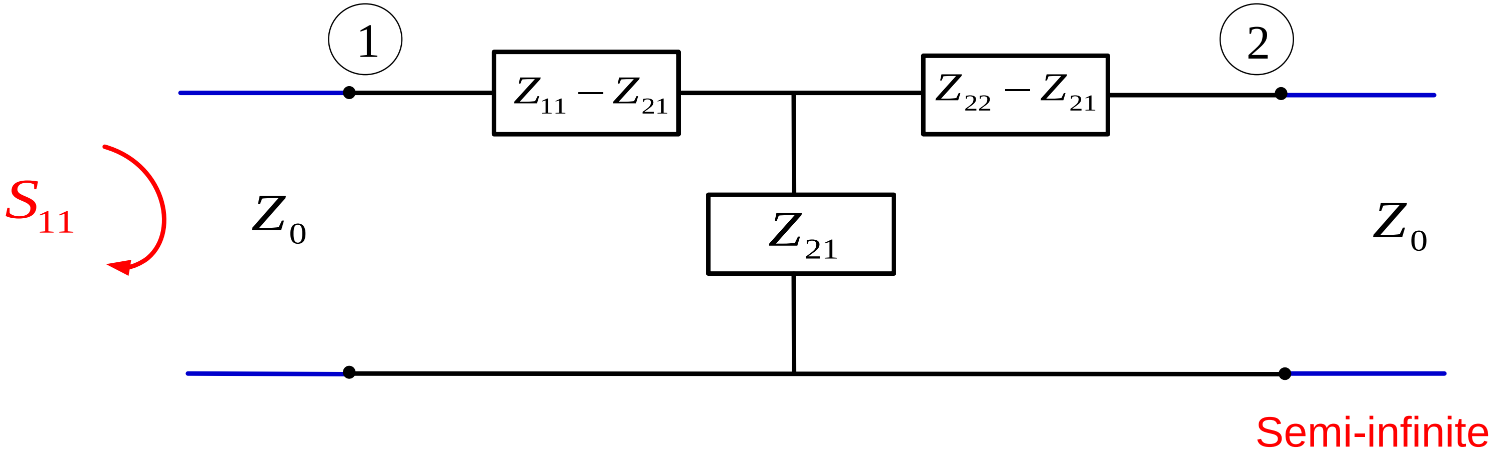
$|Z| = Z_{11}Z_{22} - Z_{12}Z_{21}$; $|Y| = Y_{11}Y_{22} - Y_{12}Y_{21}$; $\Delta Y = (Y_{11}+Y_0)(Y_{22}+Y_0) - Y_{12}Y_{21}$; $\Delta Z = (Z_{11}+Z_0)(Z_{22}+Z_0) - Z_{12}Z_{21}$; $Y_0 = 1/Z_0$.

Example

Derive S_{ij} from the Z parameters.

(The result is given inside row 1, column 2, of the previous table.)

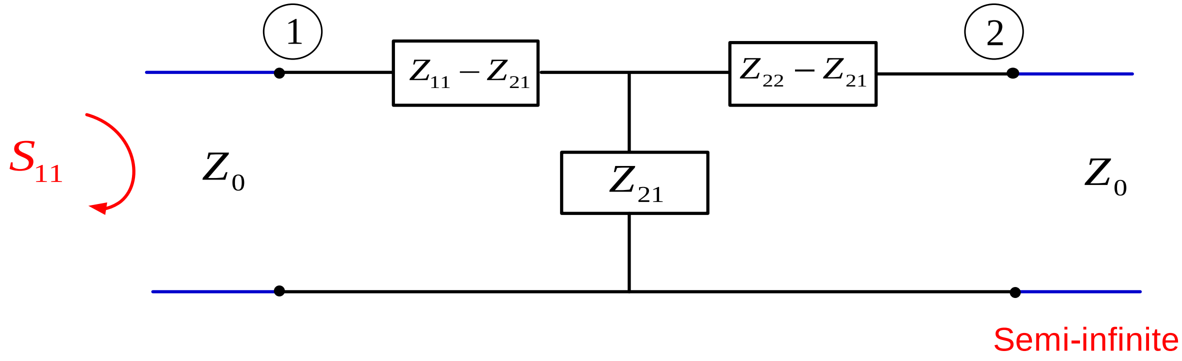
S_{11} Calculation:



$$S_{11} = \Gamma_{in1} = \frac{Z_{in} - Z_0}{Z_{in} + Z_0}$$

$$Z_{in} = (Z_{11} - Z_{21}) + (Z_{21}) \,||\, \left[(Z_{22} - Z_{21}) + Z_0\right]$$

Example (cont.)



$$Z_{in} = (Z_{11}-Z_{21}) + (Z_{21}) \,||\, \left[(Z_{22}-Z_{21}) + Z_0\right]$$

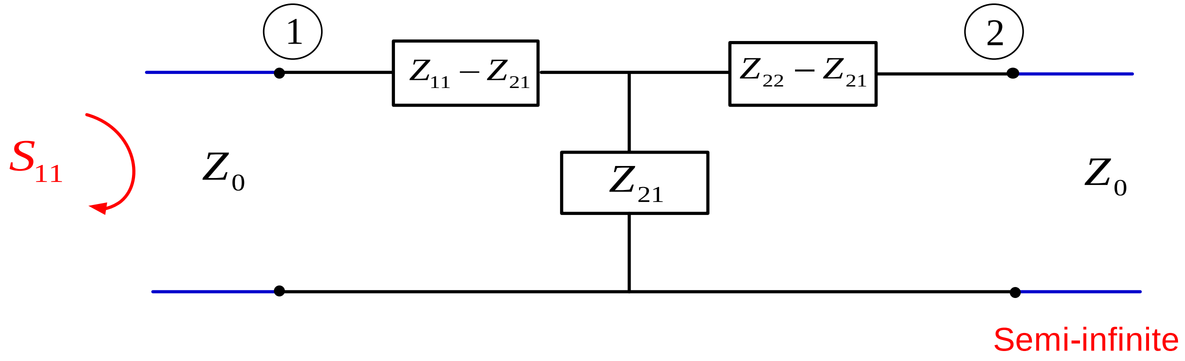
$$= (Z_{11}-Z_{21}) + \frac{Z_{21}(Z_{22}+Z_0-Z_{21})}{Z_{22}+Z_0}$$

$$= \frac{(Z_{11}-Z_{21})(Z_{22}+Z_0) + Z_{21}(Z_{22}+Z_0-Z_{21})}{Z_{22}+Z_0}$$

$$= \frac{Z_{11}Z_{22} + Z_{11}Z_0 - \cancel{Z_{21}Z_{22}} - \cancel{Z_{21}Z_0} + \cancel{Z_{21}Z_{22}} + \cancel{Z_{21}Z_0} - Z_{21}^2}{Z_{22}+Z_0}$$

$$= \frac{Z_{11}Z_{22} + Z_{11}Z_0 - Z_{21}^2}{Z_{22}+Z_0}$$

Example (cont.)



We have:

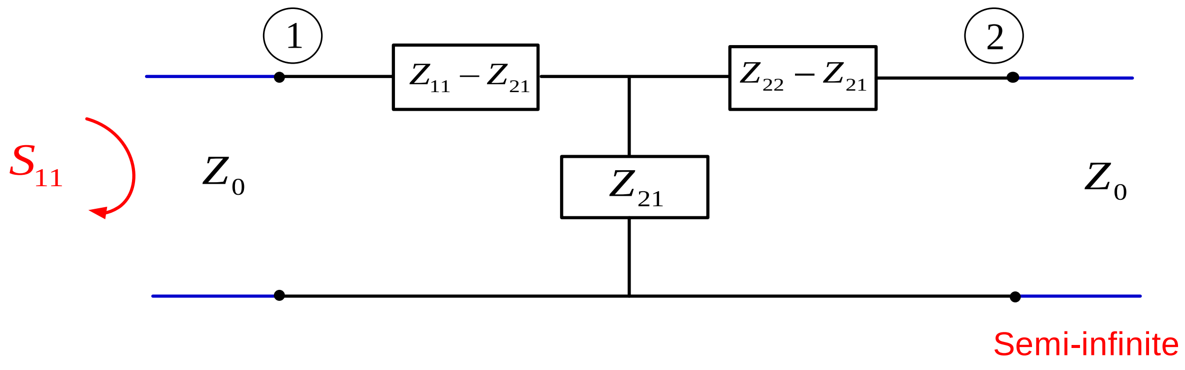
$$Z_{in}=\frac{Z_{11}\left(Z_0+Z_{22}\right)-Z_{21}^2}{Z_{22}+Z_0}$$

so

$$S_{11}=\frac{Z_{in}-Z_0}{Z_{in}+Z_0}=\frac{Z_{in}-Z_0}{Z_{in}+Z_0}\frac{\left(Z_0+Z_{22}\right)}{\left(Z_0+Z_{22}\right)}=\frac{\left(Z_{11}\left(Z_0+Z_{22}\right)-Z_{21}^2\right)-Z_0\left(Z_0+Z_{22}\right)}{\left(Z_{11}\left(Z_0+Z_{22}\right)-Z_{21}^2\right)+Z_0\left(Z_0+Z_{22}\right)}$$

We next simplify this.

Example (cont.)

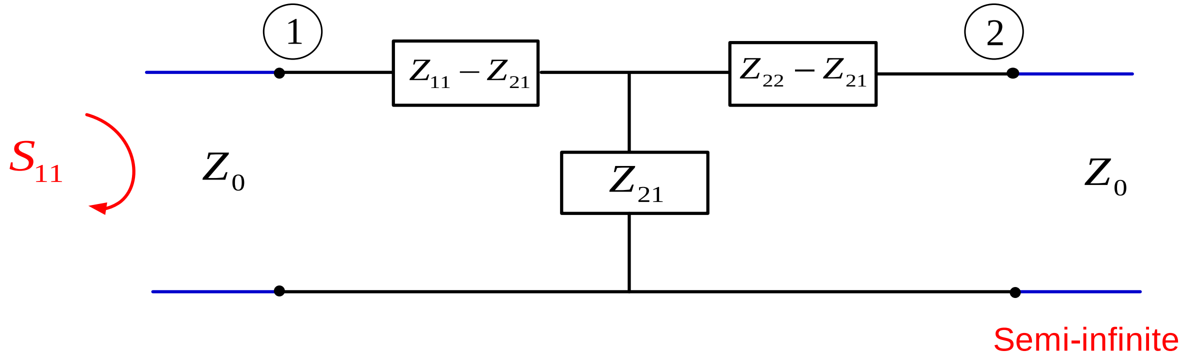


$$S_{11}=\frac{Z_{11}\left(Z_0+Z_{22}\right)-Z_{21}^2-Z_0\left(Z_0+Z_{22}\right)}{Z_{11}\left(Z_0+Z_{22}\right)-Z_{21}^2+Z_0\left(Z_0+Z_{22}\right)}$$

$$=\frac{Z_{11}Z_0+Z_{11}Z_{22}-Z_{21}^2-Z_0^2-Z_0Z_{22}}{Z_{11}Z_0+Z_{11}Z_{22}-Z_{21}^2+Z_0^2+Z_0Z_{22}}$$

$$=\frac{\left(Z_0+Z_{22}\right)\left(Z_{11}-Z_0\right)-Z_{21}^2}{\left(Z_0+Z_{22}\right)\left(Z_{11}+Z_0\right)-Z_{21}^2}$$

Example (cont.)



Hence

$$S_{11} = \frac{(Z_0 + Z_{22})(Z_{11} - Z_0) - Z_{21}^2}{(Z_0 + Z_{22})(Z_{11} + Z_0) - Z_{21}^2}$$

This agrees with the table.

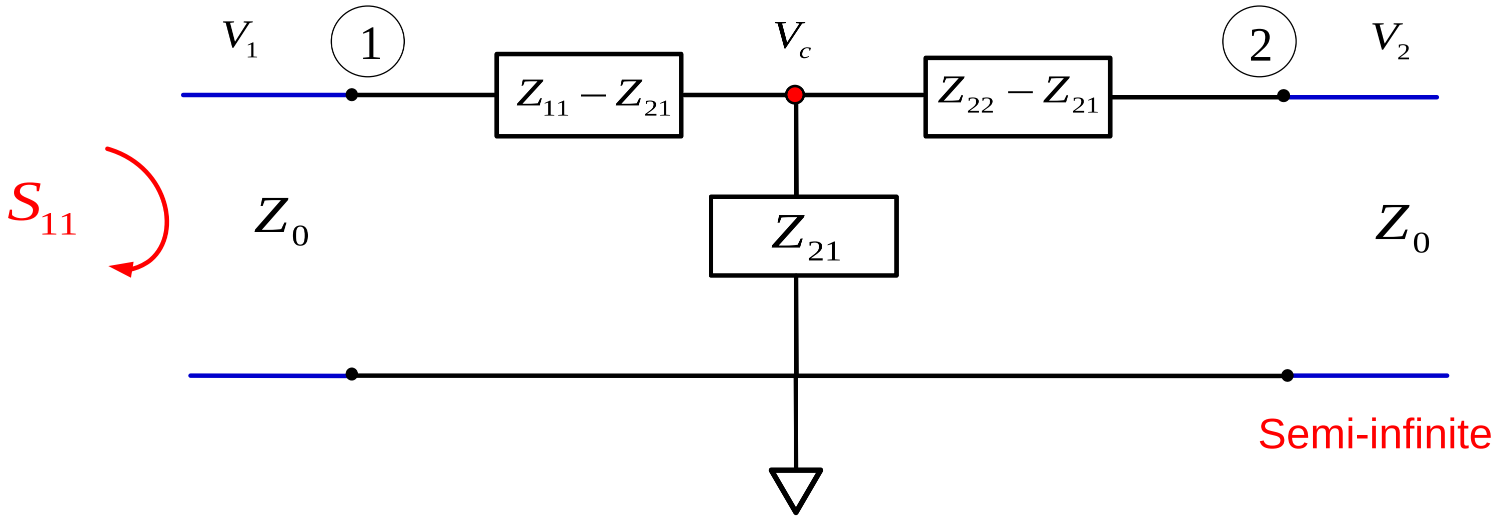
Note: To get S_{22}, simply let $Z_{11} \to Z_{22}$ in the previous result.
Hence, we have:

$$S_{22} = \frac{(Z_0 + Z_{11})(Z_{22} - Z_0) - Z_{21}^2}{(Z_0 + Z_{11})(Z_{22} + Z_0) - Z_{21}^2}$$

This agrees with the table.

Example (cont.)

S_{21} Calculation:



Assume $V_1^+(0) = 1\,[\mathrm{V}]$

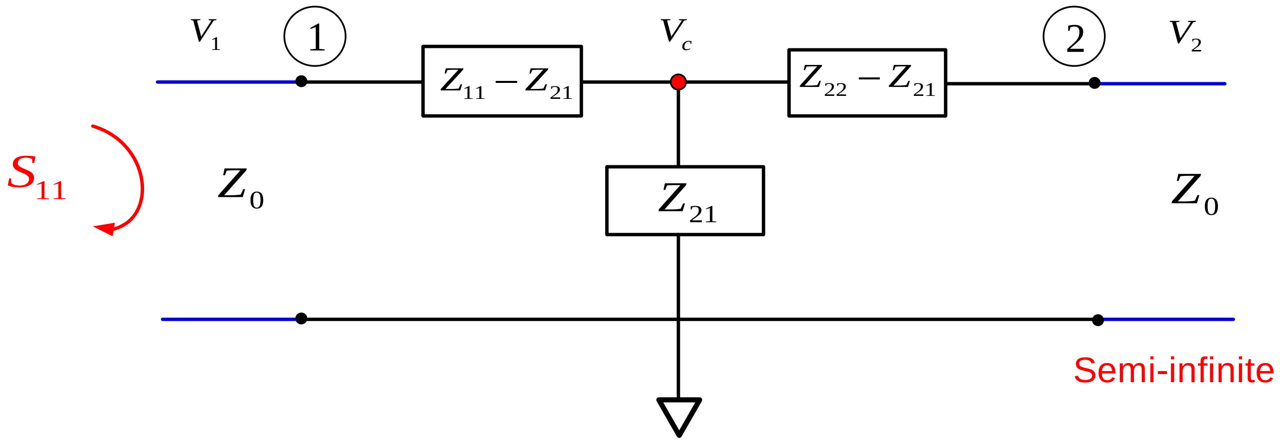
$$\Rightarrow \; S_{21} = V_2^-(0) = V_2(0)$$

Also, $V_1(0) = V_1^+(0)(1 + S_{11}) = 1 + S_{11}$

Use voltage divider equation twice to get $V_2(0)$: $V_1(0) \rightarrow V_c \rightarrow V_2(0)$

Example (cont.)

$$V_1(0) = 1 + S_{11}$$



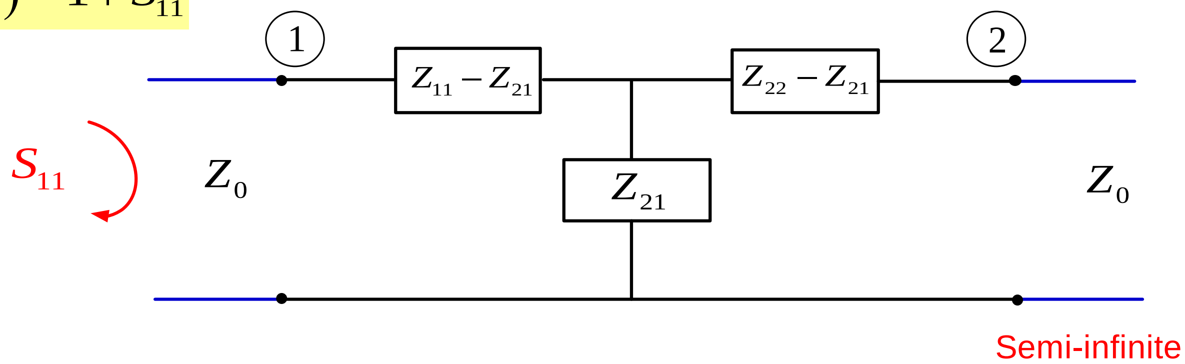
Use voltage divider equation twice:

$$V_c = V_1(0)\left(\frac{(Z_{21}) \,||\, \left[(Z_{22} - Z_{21}) + Z_0\right]}{(Z_{11} - Z_{21}) + (Z_{21}) \,||\, \left[(Z_{22} - Z_{21}) + Z_0\right]}\right)$$

$$V_2(0) = V_c\left(\frac{Z_0}{(Z_{22} - Z_{21}) + Z_0}\right)$$

Example (cont.)

$V_1(0) = 1 + S_{11}$



Hence

$$S_{21} = V_2(0) = (1 + S_{11}) \left(\frac{(Z_{21}) \,||\, \left[(Z_{22} - Z_{21}) + Z_0 \right]}{(Z_{11} - Z_{21}) + (Z_{21}) \,||\, \left[(Z_{22} - Z_{21}) + Z_0 \right]} \right) \left(\frac{Z_0}{(Z_{22} - Z_{21}) + Z_0} \right)$$

where

$$1 + S_{11} = 1 + \frac{(Z_0 + Z_{22})(Z_{11} - Z_0) - Z_{21}^2}{(Z_0 + Z_{22})(Z_{11} + Z_0) - Z_{21}^2}$$

Example (cont.)

Our result:

$$S_{21} = (1+S_{11})\left(\frac{(Z_{21})\,||\left[(Z_{22}-Z_{21})+Z_0\right]}{(Z_{11}-Z_{21})+(Z_{21})\,||\left[(Z_{22}-Z_{21})+Z_0\right]}\right)\left(\frac{Z_0}{(Z_{22}-Z_{21})+Z_0}\right)$$

where

$$1+S_{11} = 1+\frac{(Z_0+Z_{22})(Z_{11}-Z_0)-Z_{21}^2}{(Z_0+Z_{22})(Z_{11}+Z_0)-Z_{21}^2}$$

After simplifying, we should get the result in the table:

(You are welcome to check it!)

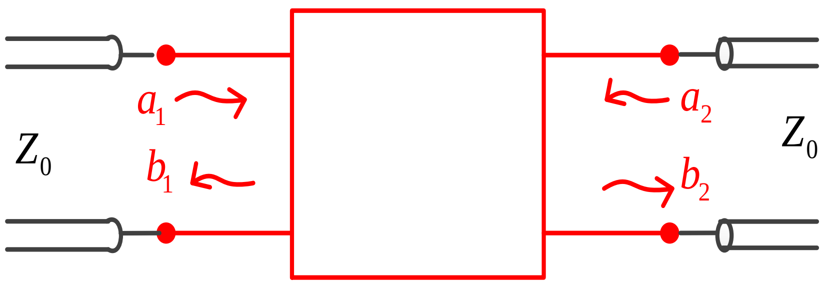
$$S_{21} = S_{21} = \frac{2Z_{12}Z_0}{(Z_0+Z_{22})(Z_{11}+Z_0)-Z_{21}^2}$$

This is the result in the table.

Signal-Flow Graph

This is way to graphically represent S parameters.

Please see the Pozar book for more details.

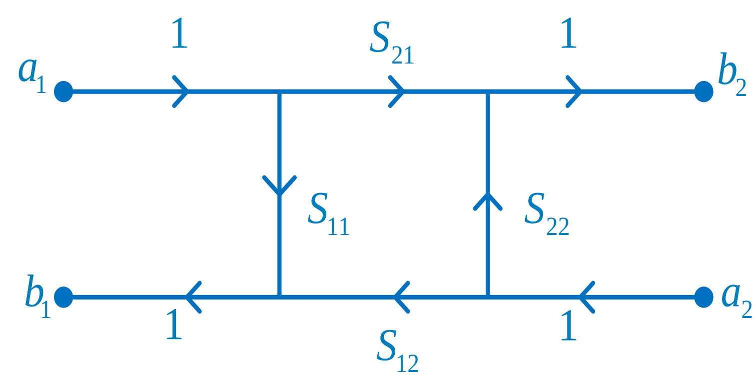


The wave amplitudes are represented as <u>nodes</u> in the single-flow graph.

$$b_1 = S_{11}a_1 + S_{12}a_2$$
$$b_2 = S_{21}a_1 + S_{22}a_2$$

(wave amplitudes evaluated at $z_i = 0$)

$\Rightarrow$



Rule: The value at each node is the sum of the values coming into the node from the various other nodes.